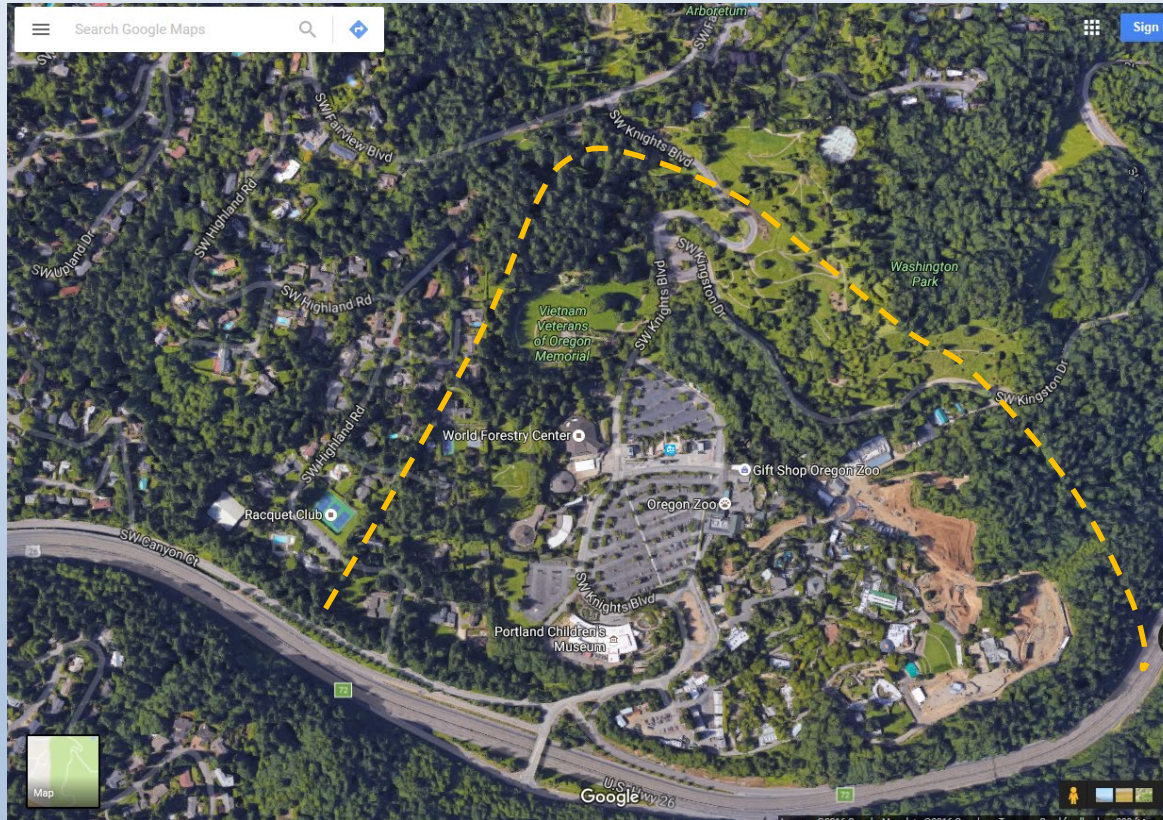


Slope Stabilization Case Studies

Learning Objectives

- Introduce several instructive case studies that illustrate the concepts of landslide repair.

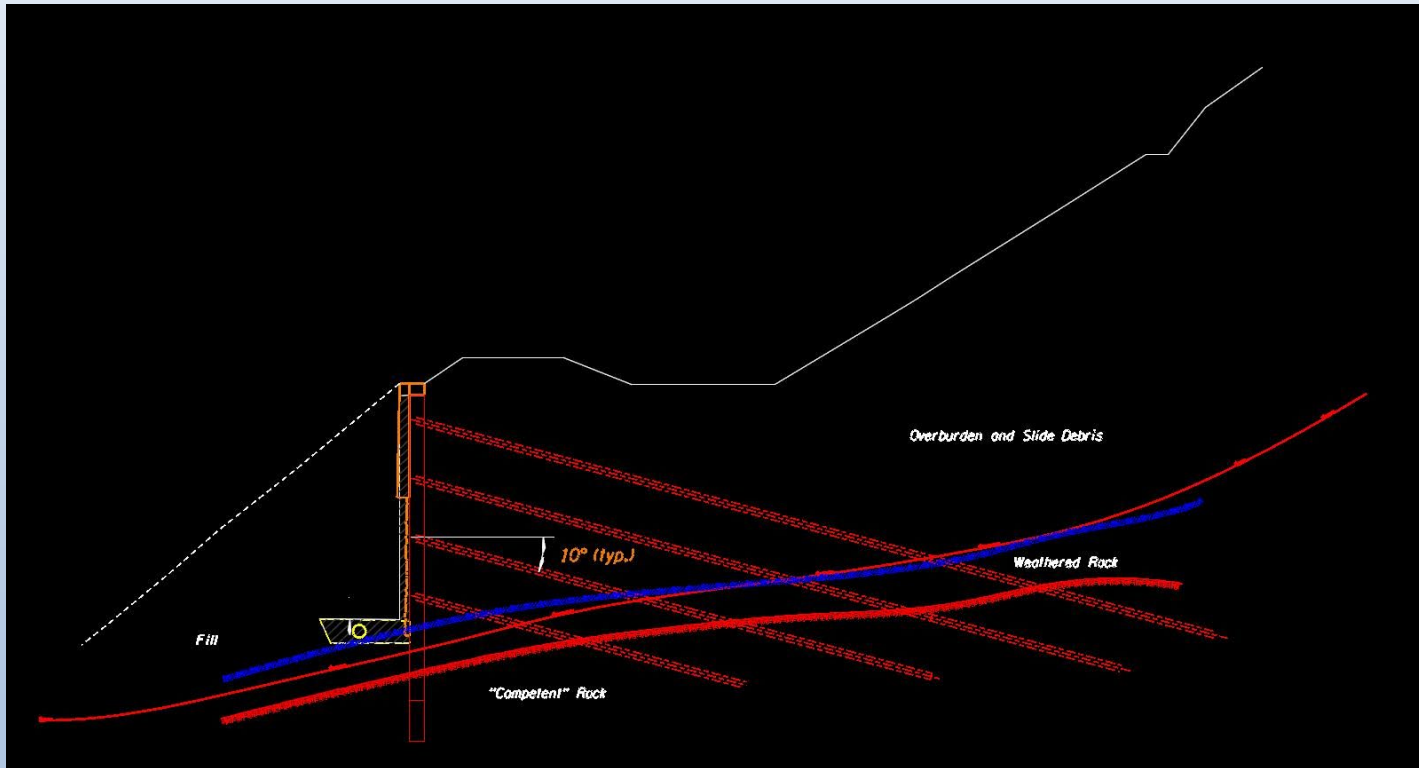
Zoo-Highlands Slide



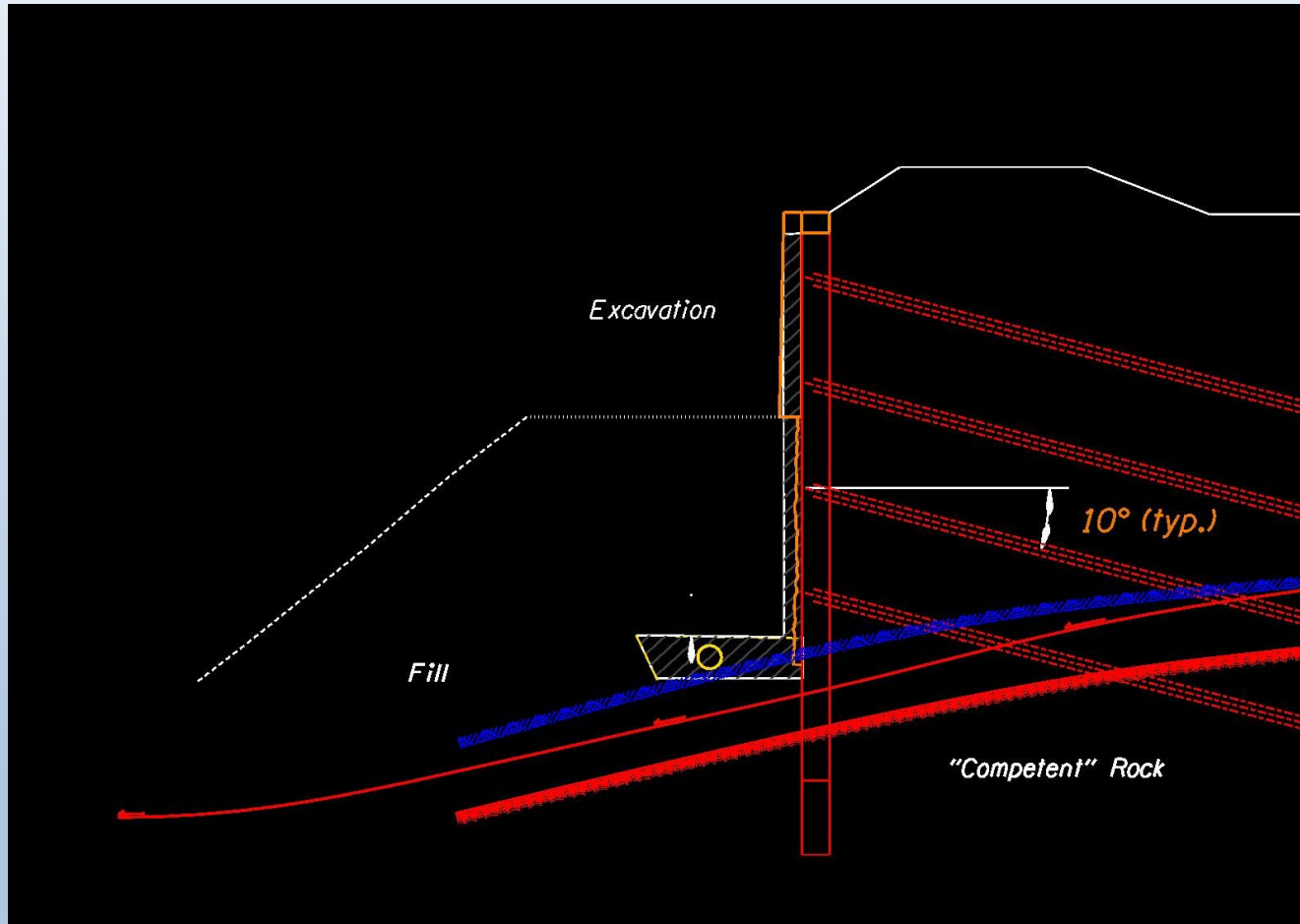
Exploration Program



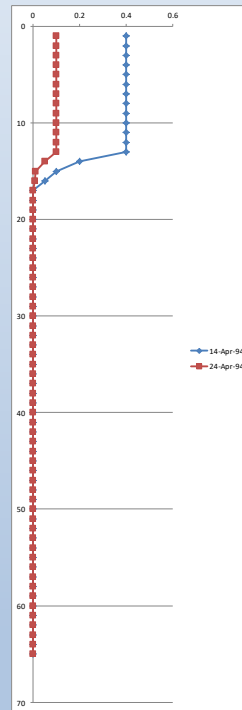
Tieback Wall (General Plan)



Over-Excavation/Out-of-Sequence



Cautionary Results of Over-Excavation



Soldier Pile Drilling & Installation



Tieback Drilling



Tieback Installation



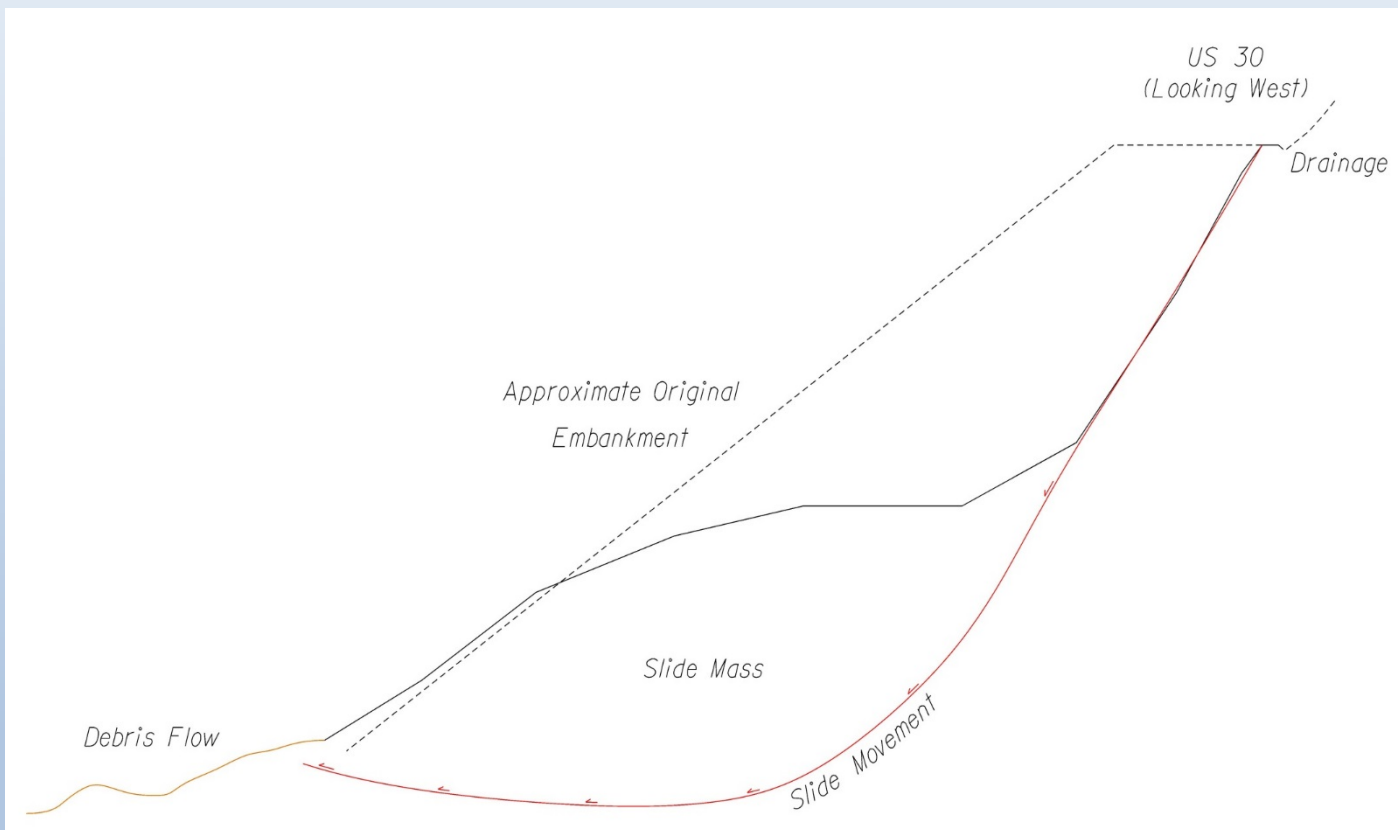
Near-Completion



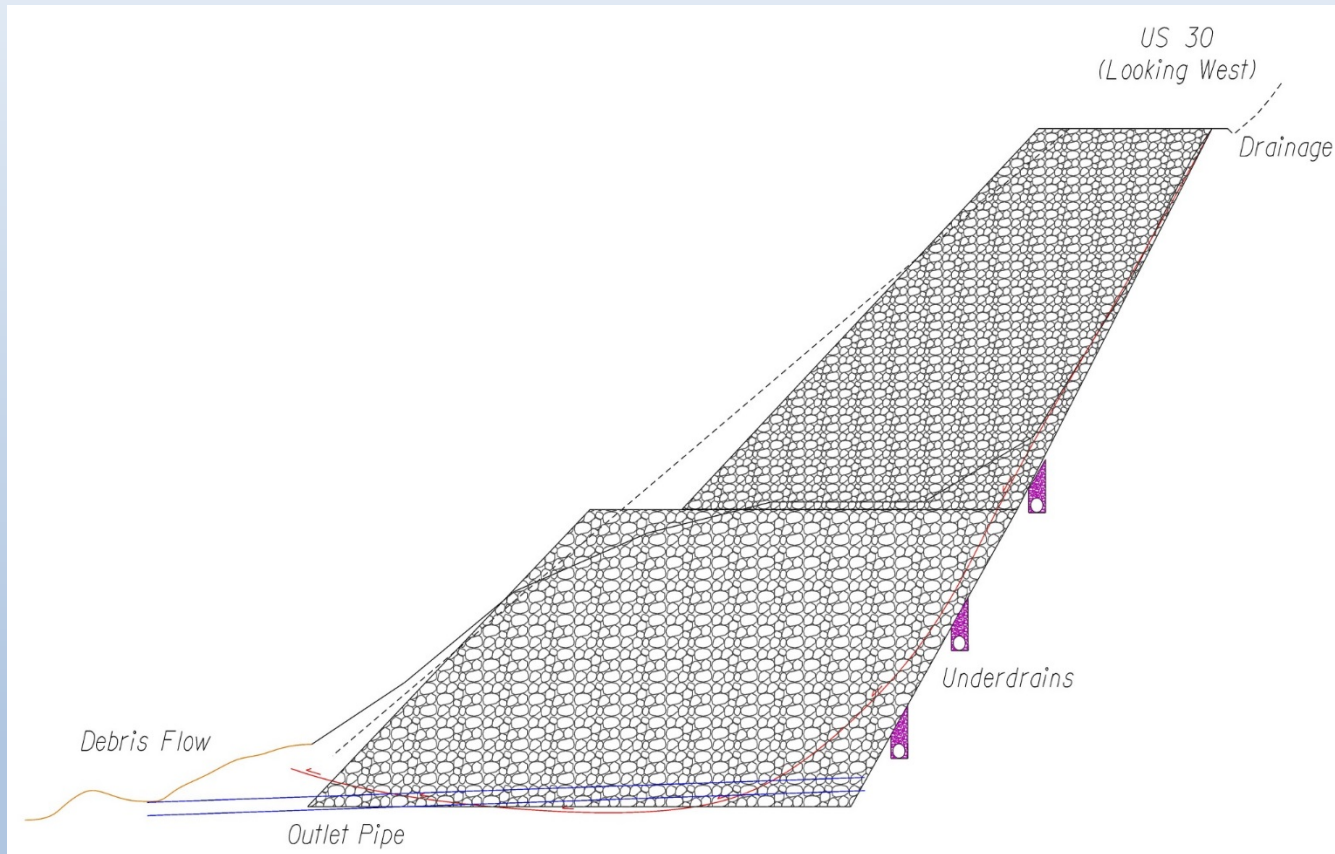
US 30 @ Clatskanie



Initial Failure



Repair Schematic



Buttress/Shear Key Excavation



Underdrains



Finished Embankment





SLOPE STABILIZATION CASE STUDIES IN A FOREST ENVIRONMENT

WFCA April 11-12, 2019 RAR

“Typical Landslide, Cut/Fill Slope Problems Encountered on Low Volume Roads in Steep Mountainous Terrain and Their Solutions”

Courtesy of: Ed Rose (Retired)
R1 Geotechnical Engineer

General Categories of Problems Created by Road Building

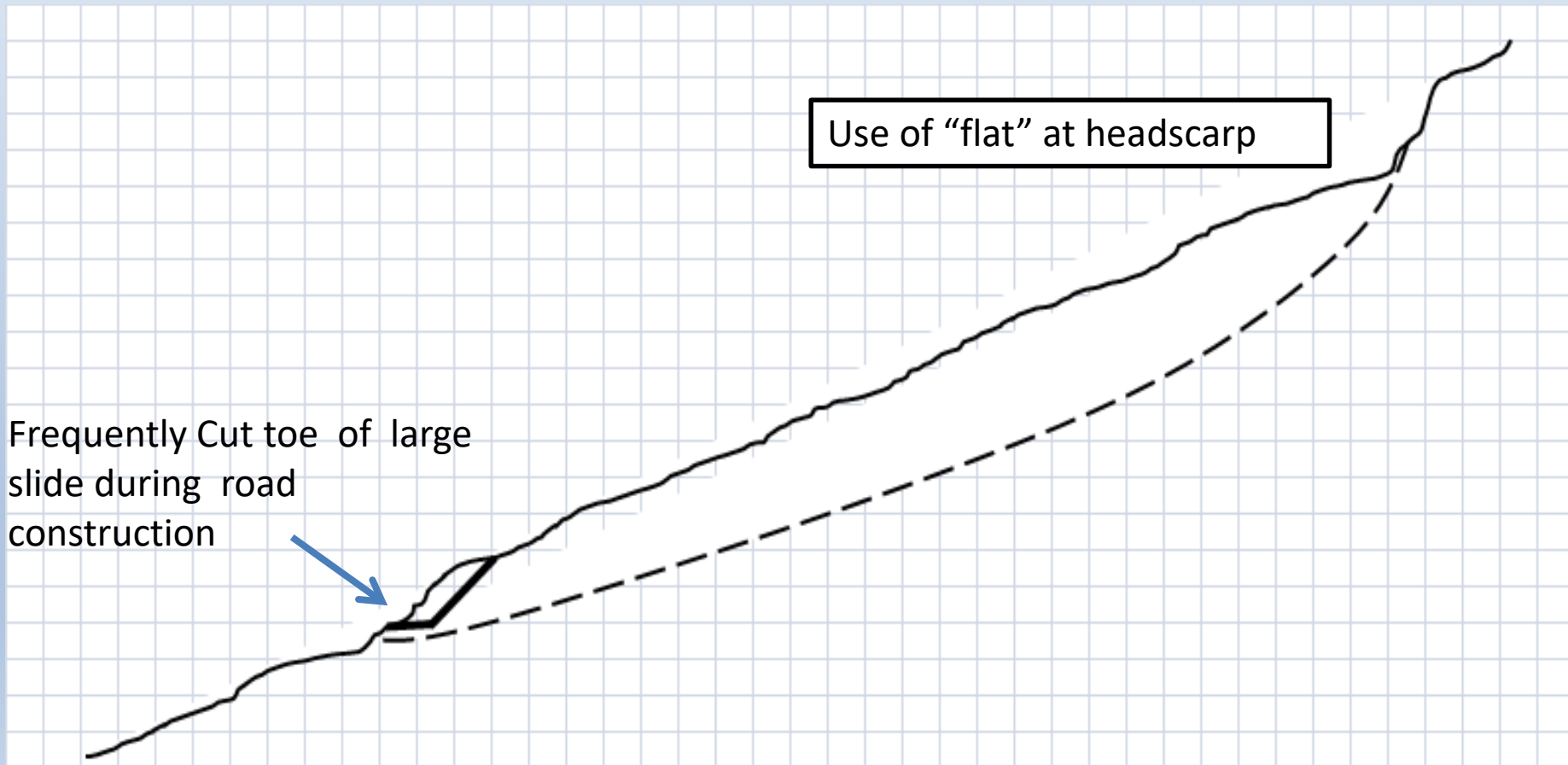
- Large ancient landslides disturbed by cutting or filling
- Smaller deposits of colluvium, residual soil, fault zones or glacial deposits disturbed
 - Cutting creating unstable cutslopes
 - Filling creating unstable fill/ground
 - Altering natural hydrology/groundwater (increased groundwater under fill)
- Side-cast fill with organics remaining

Legacy Forest Service Road -1964

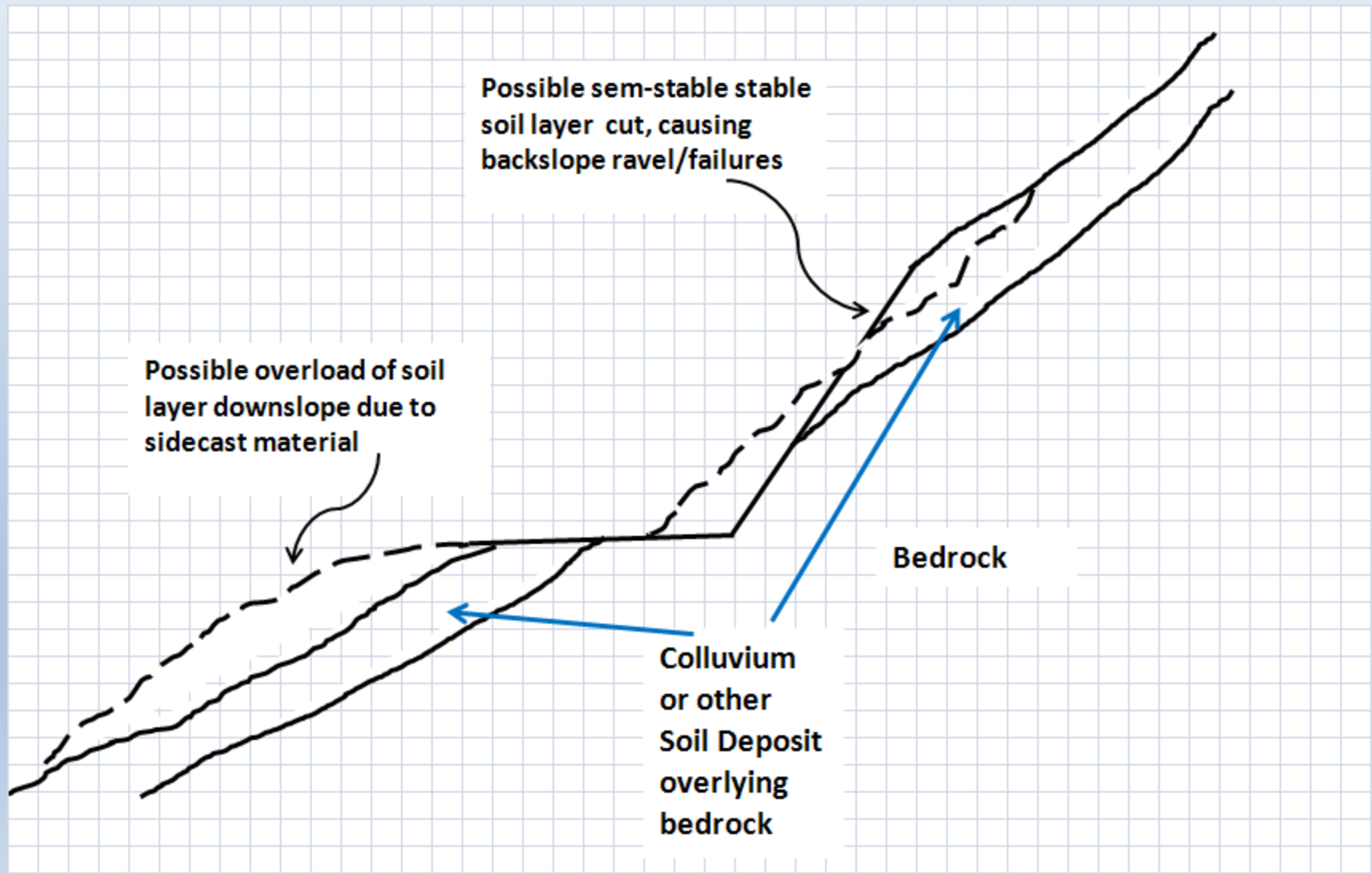
Typical Side –Cast Construction



Ancient Landslide Terrain



Frequent Full-Bench Road Construction Impacts



Implement Cost Effective Solution

3-Step process

- Investigate and define problem-
 - Establish boundary conditions
 - Establish materials parameters
 - Establish water table
- Geotechnical Engineering Analysis-
 - Analyze existing condition
 - Analyze possible solutions
 - Select most cost effective solution
- Prepare Design, Plans and Specifications

Investigate and Define Problem

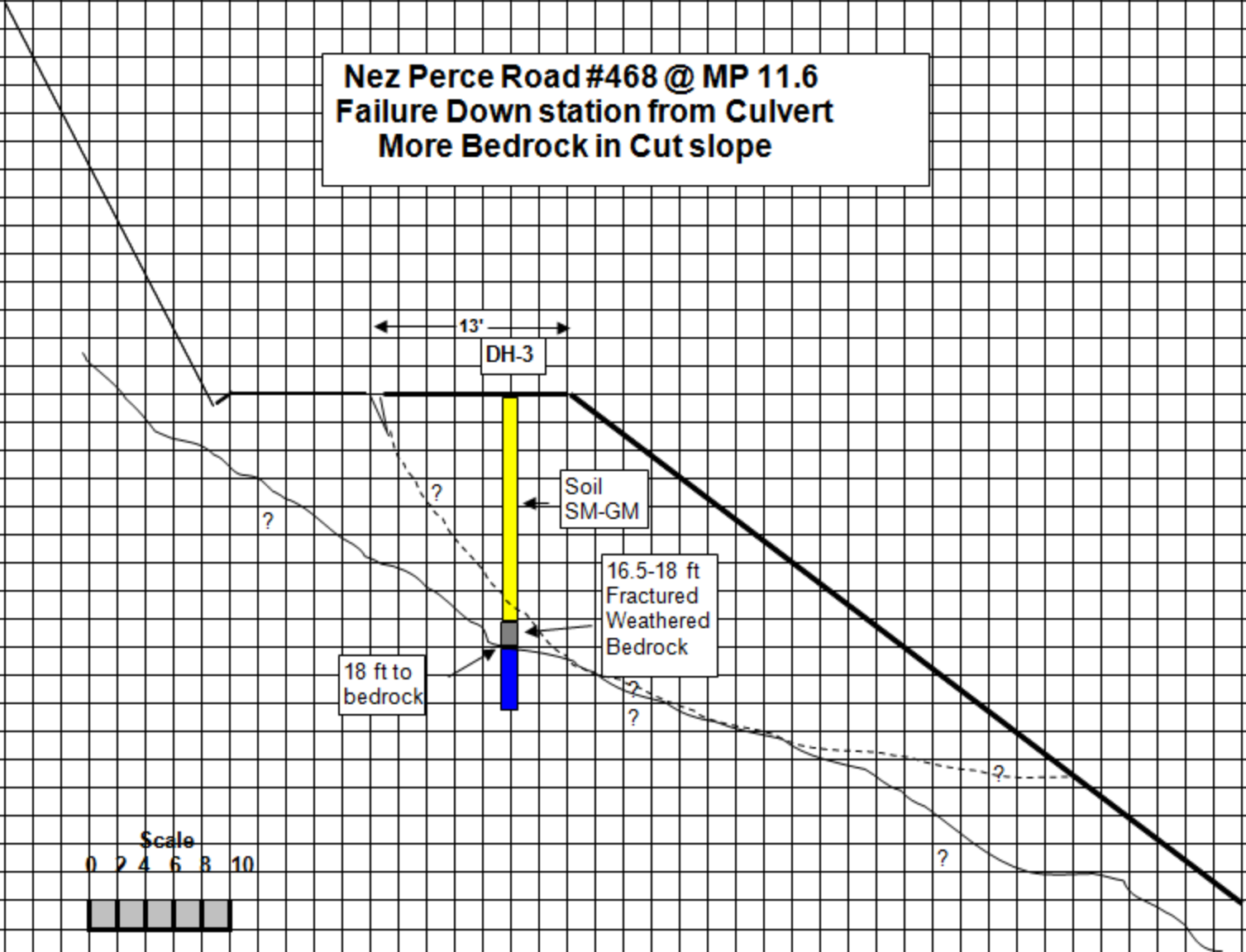
- Define boundary conditions and materials parameters
 - Reconnaissance- establish landform, strata and deposits, and identify any discontinuities (Geologist)
 - Investigation (Geologist and Engineer)
 - Surficial –Shallow hand excavations
 - At Depth – Backhoe or Drill
 - Testing Field
 - » Portable Triggs SPT, seismograph survey, vane shear, tube densities.
 - » Slope Inclinator
 - » SPT, splitspoon samples, shelly tube samples
 - Laboratory tests
 - » Classification, moisture, density
 - » Shear strength- direct shear/ triaxial shear
 - » Permeability
 - Establish X-Section for Analysis

Establish Critical X-Section For Analysis

- Geometry and Layering
 - depth/thickness of various strata or deposits
- Materials parameters of each layer
 - Unit weight – γ_{moist} pcf
 - Friction Angle- ϕ degrees
 - Cohesion- c psf
- Define Water table if present
 - Unit weight s– $\gamma_{\text{sat.}}$ and γ_{water}

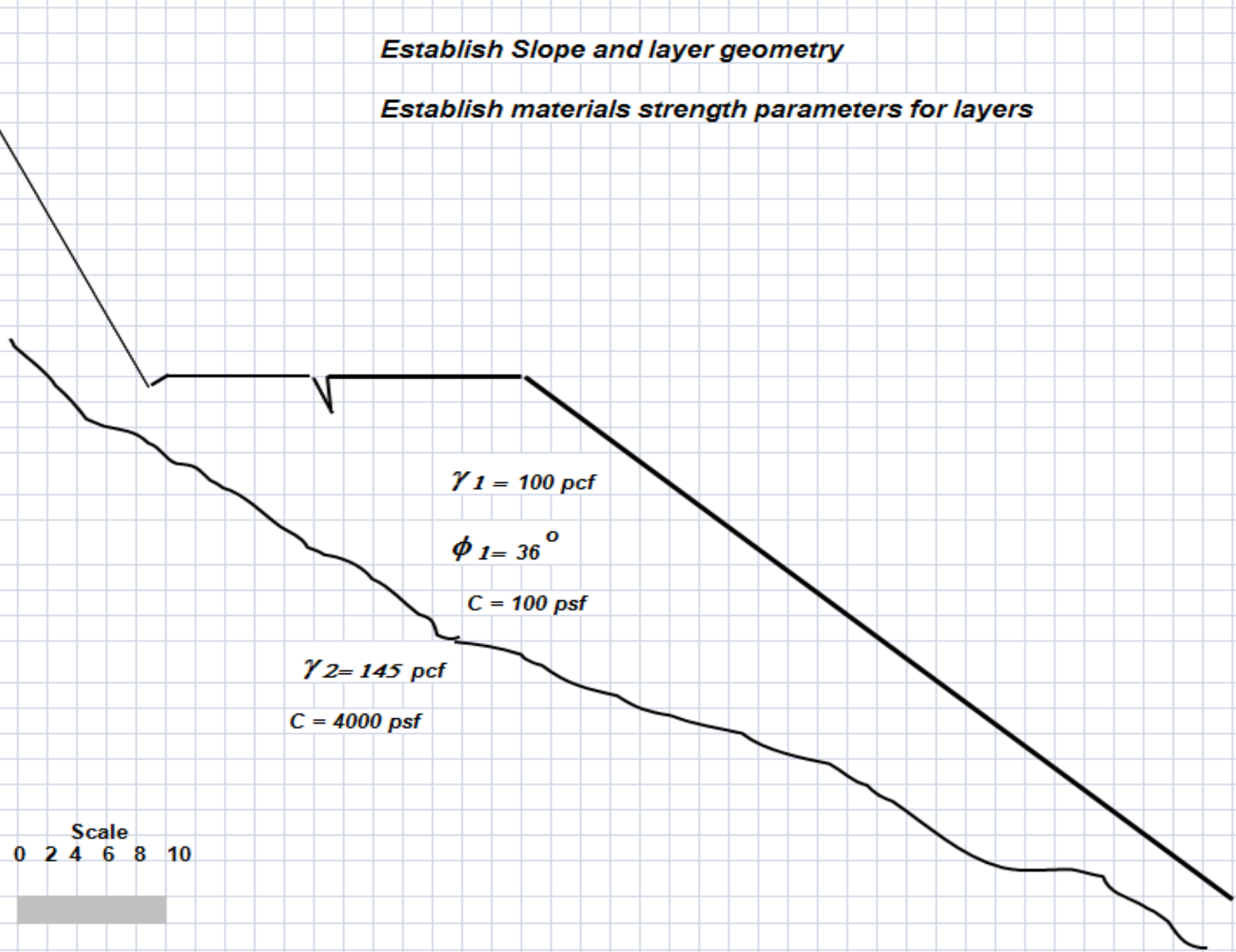
From Drill Hole and/or other Investigations

Nez Perce Road #468 @ MP 11.6
Failure Down station from Culvert
More Bedrock in Cut slope



Establish Slope and layer geometry

Establish materials strength parameters for layers



$\gamma_1 = 100 \text{ pcf}$

$\phi_1 = 36^\circ$

$C = 100 \text{ psf}$

$\gamma_2 = 145 \text{ pcf}$

$C = 4000 \text{ psf}$

Scale

0 2 4 6 8 10



RETAINING WALLS

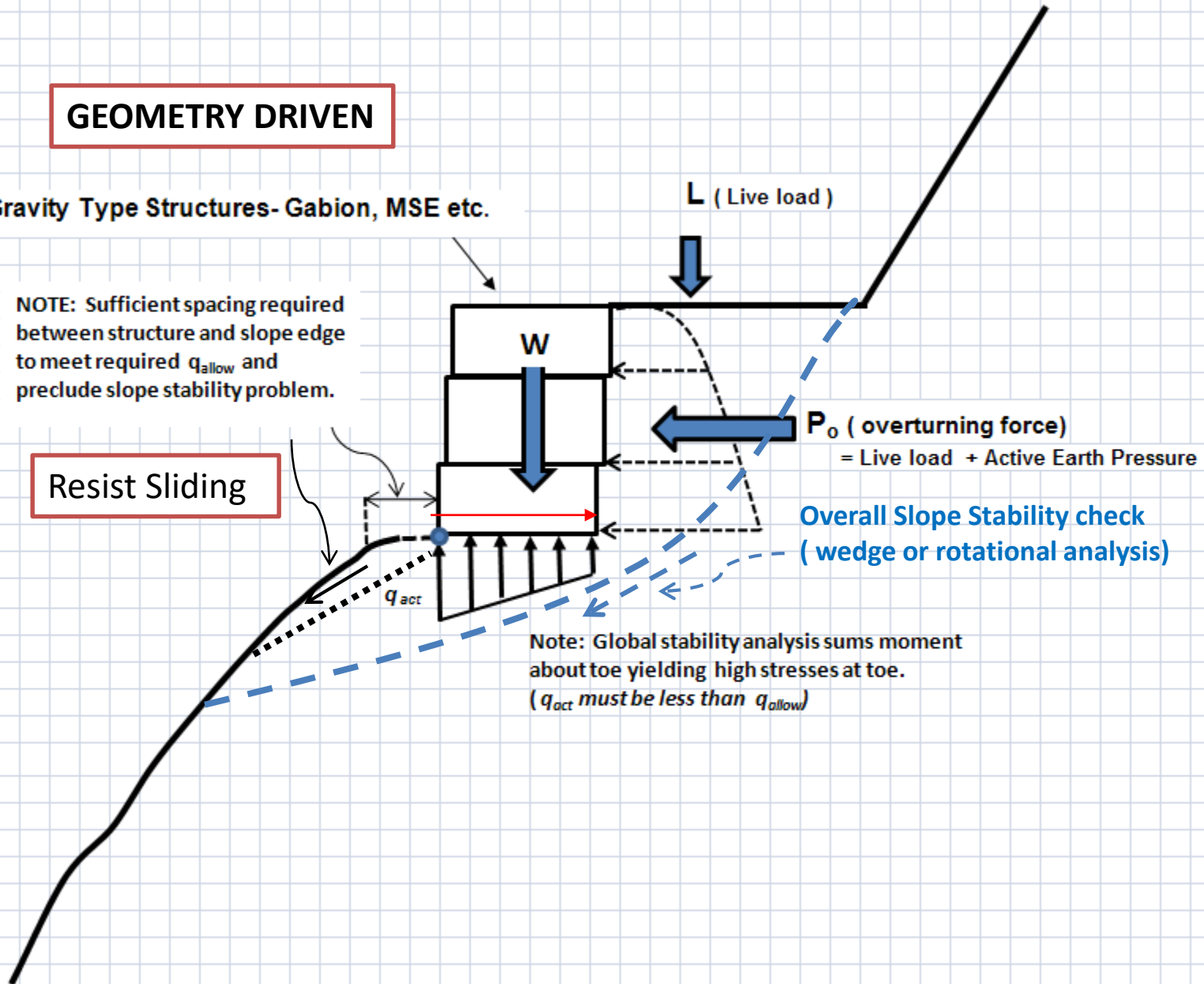


GEOMETRY DRIVEN

Gravity Type Structures- Gabion, MSE etc.

NOTE: Sufficient spacing required between structure and slope edge to meet required q_{allow} and preclude slope stability problem.

Resist Sliding



Overall Slope Stability check
(wedge or rotational analysis)

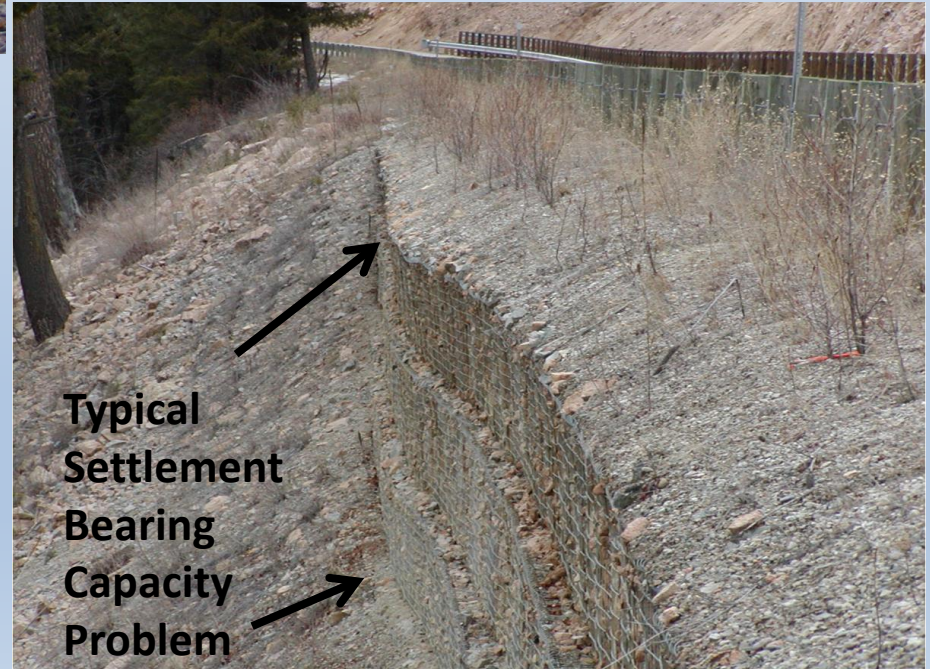
Note: Global stability analysis sums moment about toe yielding high stresses at toe.
(q_{act} must be less than q_{allow})

Gravity Type Walls

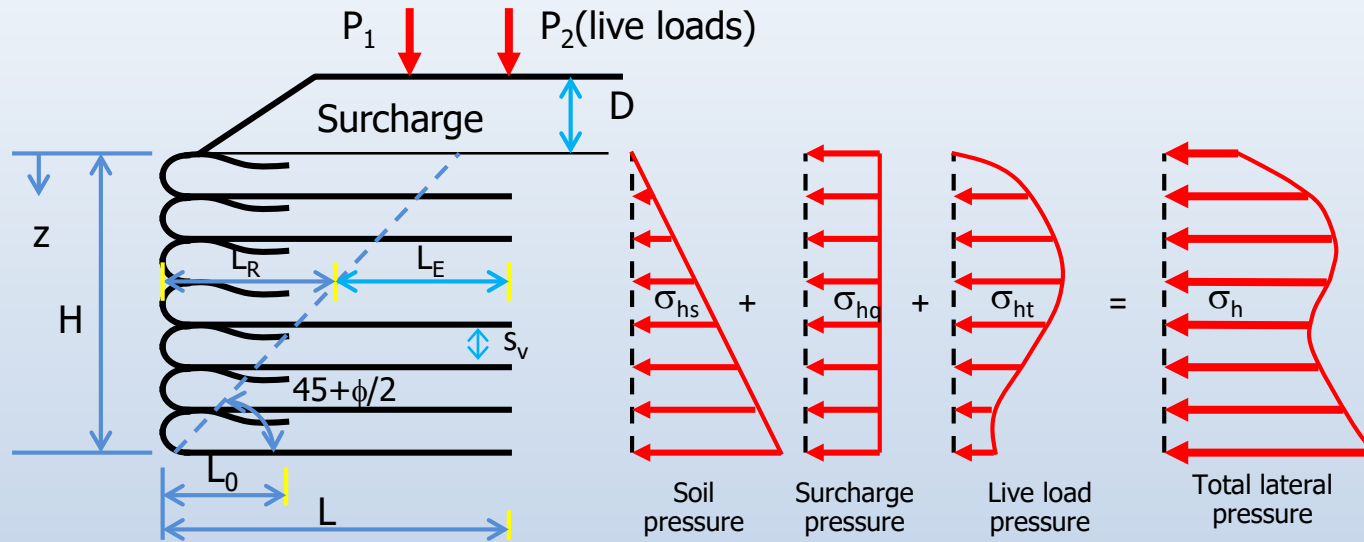
Rock Gabions



**Gabion wall at
reclaimed mine
site on Klamath
N.F. Region 5**



Elements of Basic Mechanically Stabilized Earth Wall Design



Hilfiker Welded Wire Wall-Mendocino N.F. Region 5



Angeles N.F. Region 5 Geogrid Reinforced Modular Block Wall

MSE Walls-Layered Construction



**Timber Faced Geogrid Reinforced Wall, Happy
Camp R.D. Klamath N.F.**



Timber Faced Geogrid Reinforced MSE Wall



MSE Wall Just after Completion



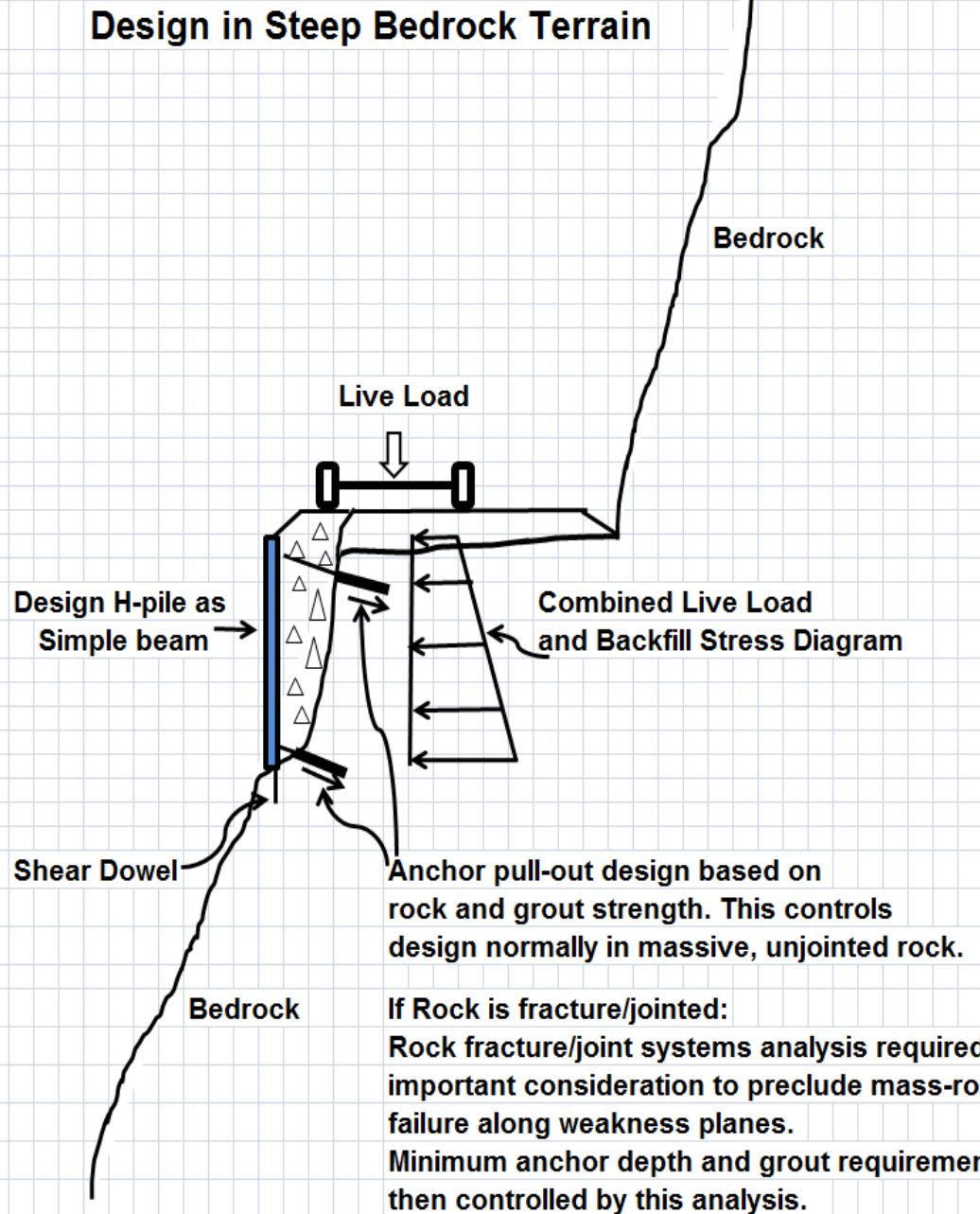
**MSE Wall 3 Years after Construction.
Happy Camp R.D. averages between 60
and 80 inches of precipitation per year**

Pile/Lagging Tie-back Component Design Ideal in Steep Bedrock Terrain

- Allows one to fit component design to terrain rather than try to modify terrain to fit structure.
- Quite often try to fit MSE wall or other gravity type structure in to bedrock
 - Needless rock excavation because of base width requirement
 - Environmental impact!

Tie-Back, H-Pile Retaining Wall

Basic Design Procedure



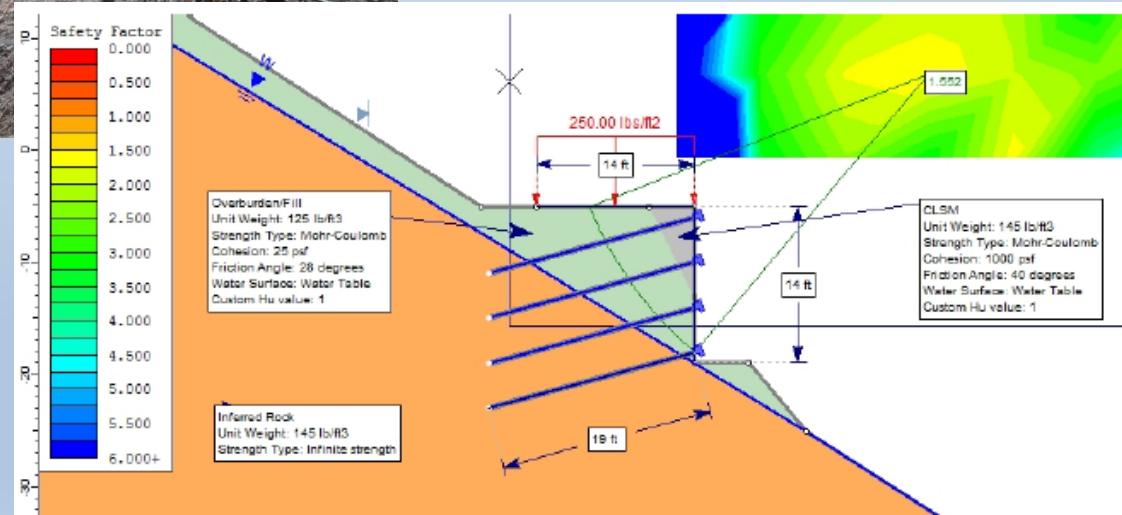
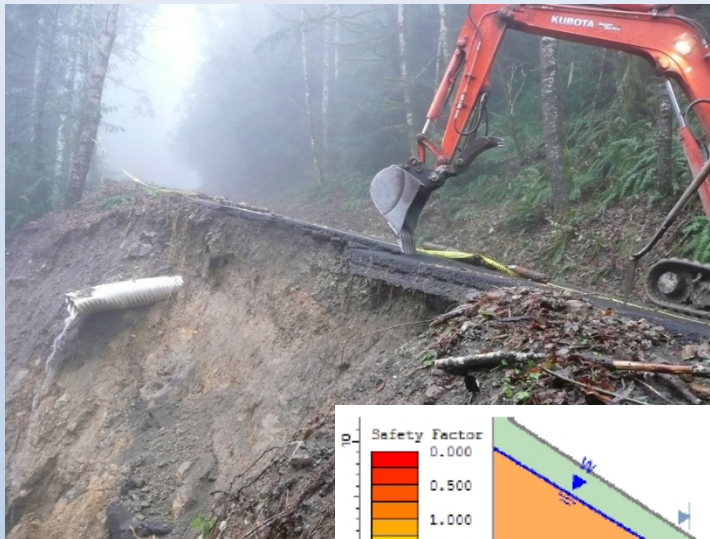


**“Component” Tie-back H-pile wall
– allows for fitting Structure to
the Terrain.
Insignificant excavation and
environmental damage!**



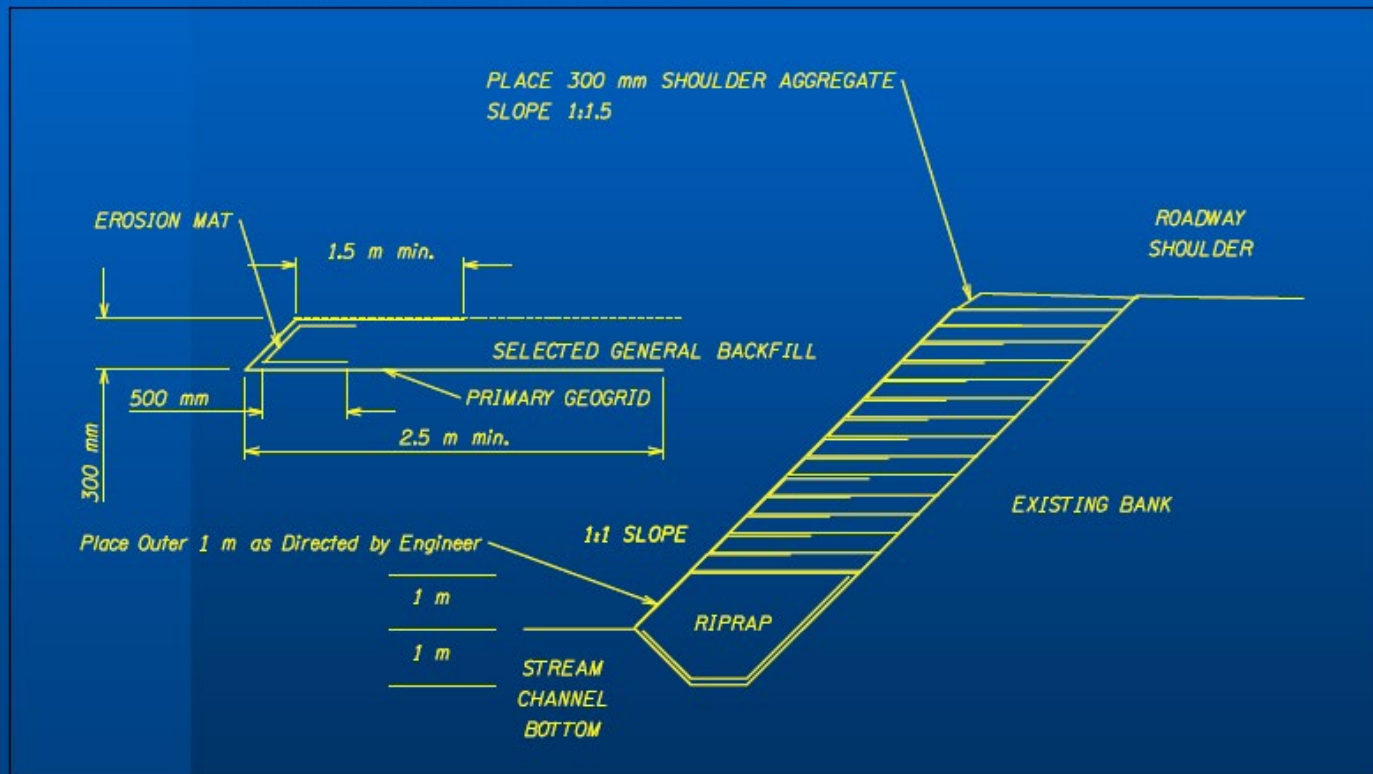
Soil Nail Anchored Wall

(Built from remaining roadway - GSI)



STABILIZATION W/GEOSYNTHETICS

Vegetated Geogrid





Variety of Geogrid products used in MSE (Mechanically Stabilized Earth) Walls and RSS (Reinforced Soil Slopes) A.K.A. Reinforced Fills.

Tensar BX 1100 + Typical used in MSE Wall Construction

Typical Over Steepened Fill Failures - Klamath N.F. Region 5

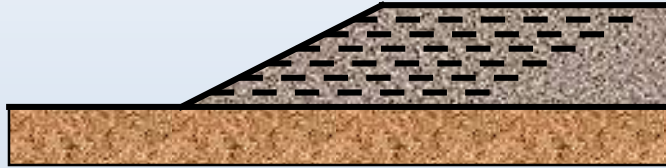


Ukonom Ranger District

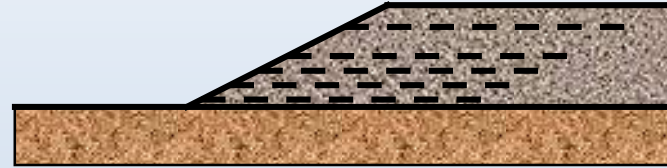


Oak Knoll Ranger District

Placement Patterns Reinforced Fill Designs



(a) Even spaced-even length



(b) Uneven spaced-even length



Primary Geogrid Reinforced Fill Layer



**Secondary Geogrid Reinforced Fill Layer.
Essential compaction of Soil for Strength**

45 ft High Reinforced Fill Ukonom R.D. Klamath N.F. Region 5



**Completed reinforced fill before
erosion control mat placed on slope**



Reinforced fill 2 years after completion.

20 Ft. High Reinforced Fill, Oak Knoll Ranger District, Klamath N.F.



Reinforced Fill Just Completed and Before Erosion Control Mat Placed on Slope.

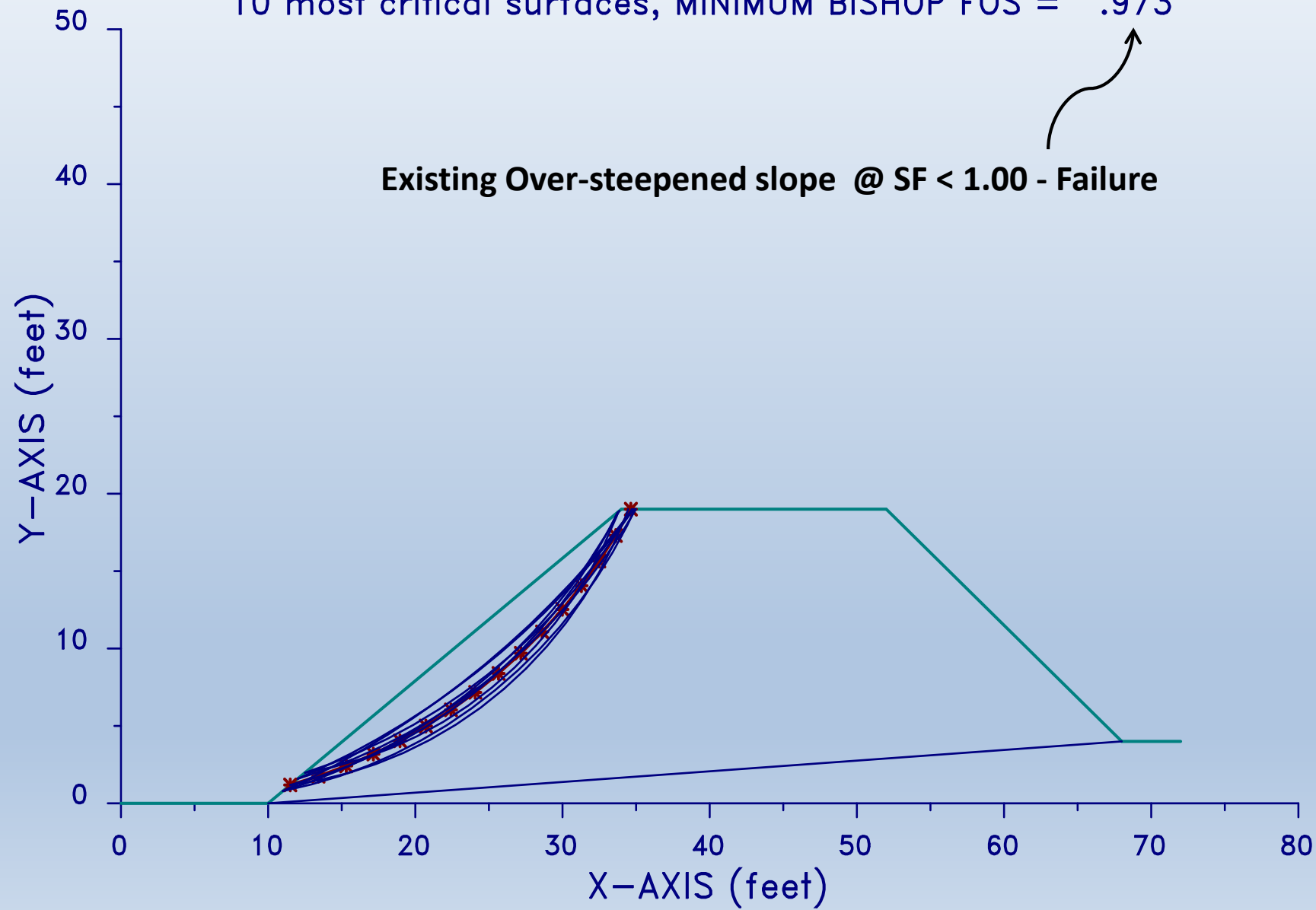


Reinforced Fill 3 years after Construction

Reinforced Fill reconstruction

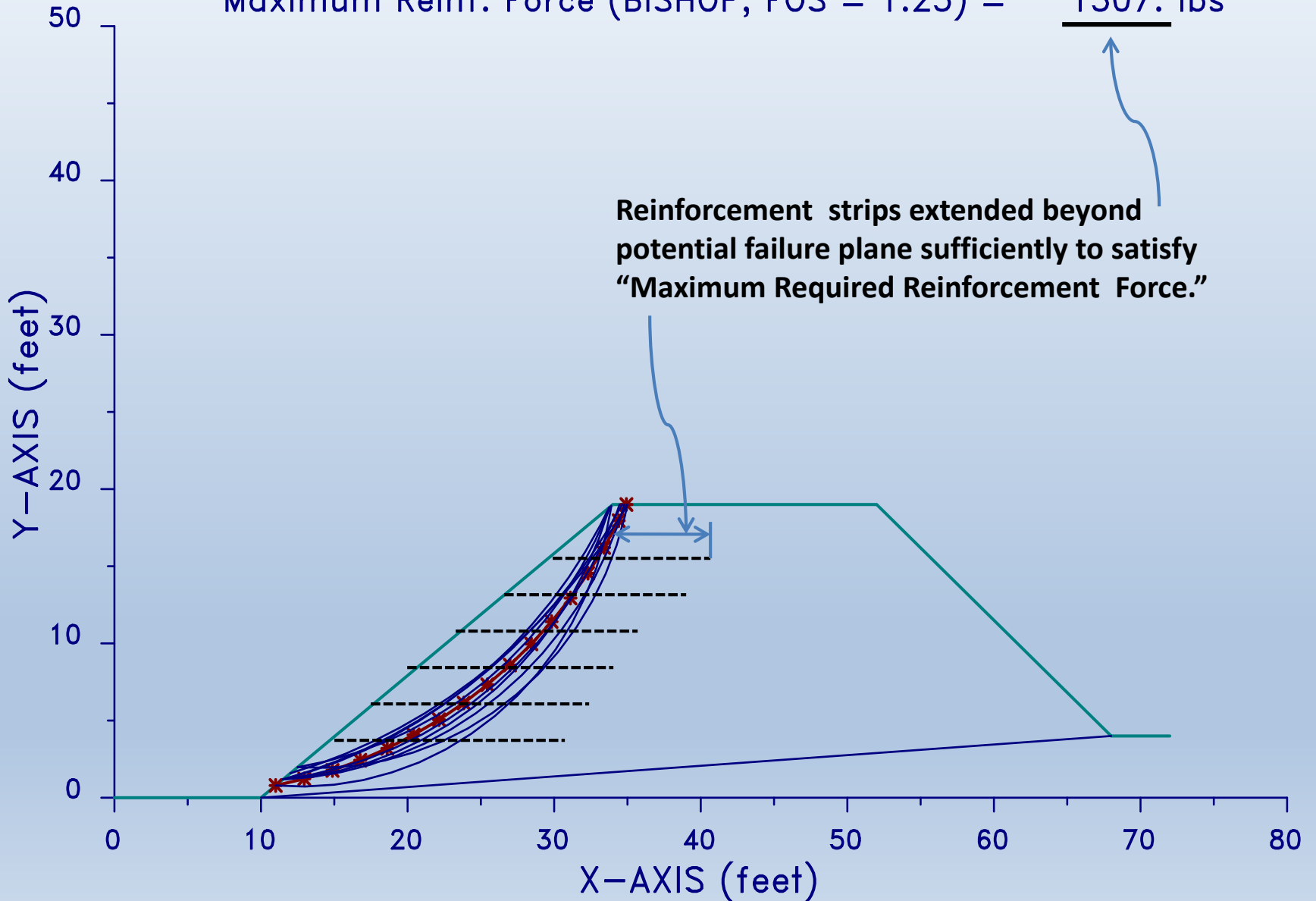
10 most critical surfaces, MINIMUM BISHOP FOS = .973

Existing Over-steepened slope @ SF < 1.00 - Failure



Reinforced Fill reconstruction

Maximum Reinf. Force (BISHOP, FOS = 1.25) = 1307. lbs



United States
Department of Agriculture

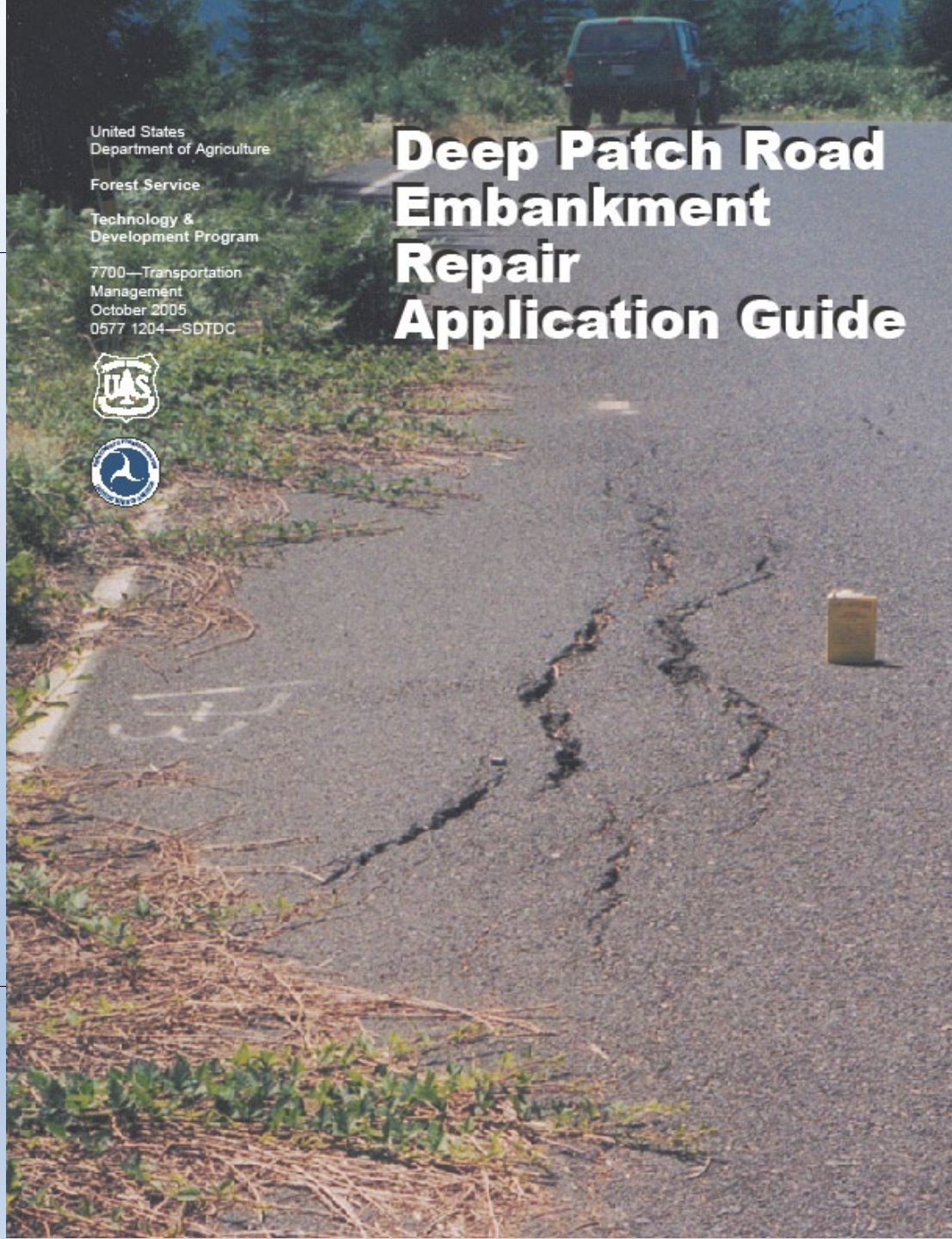
Forest Service

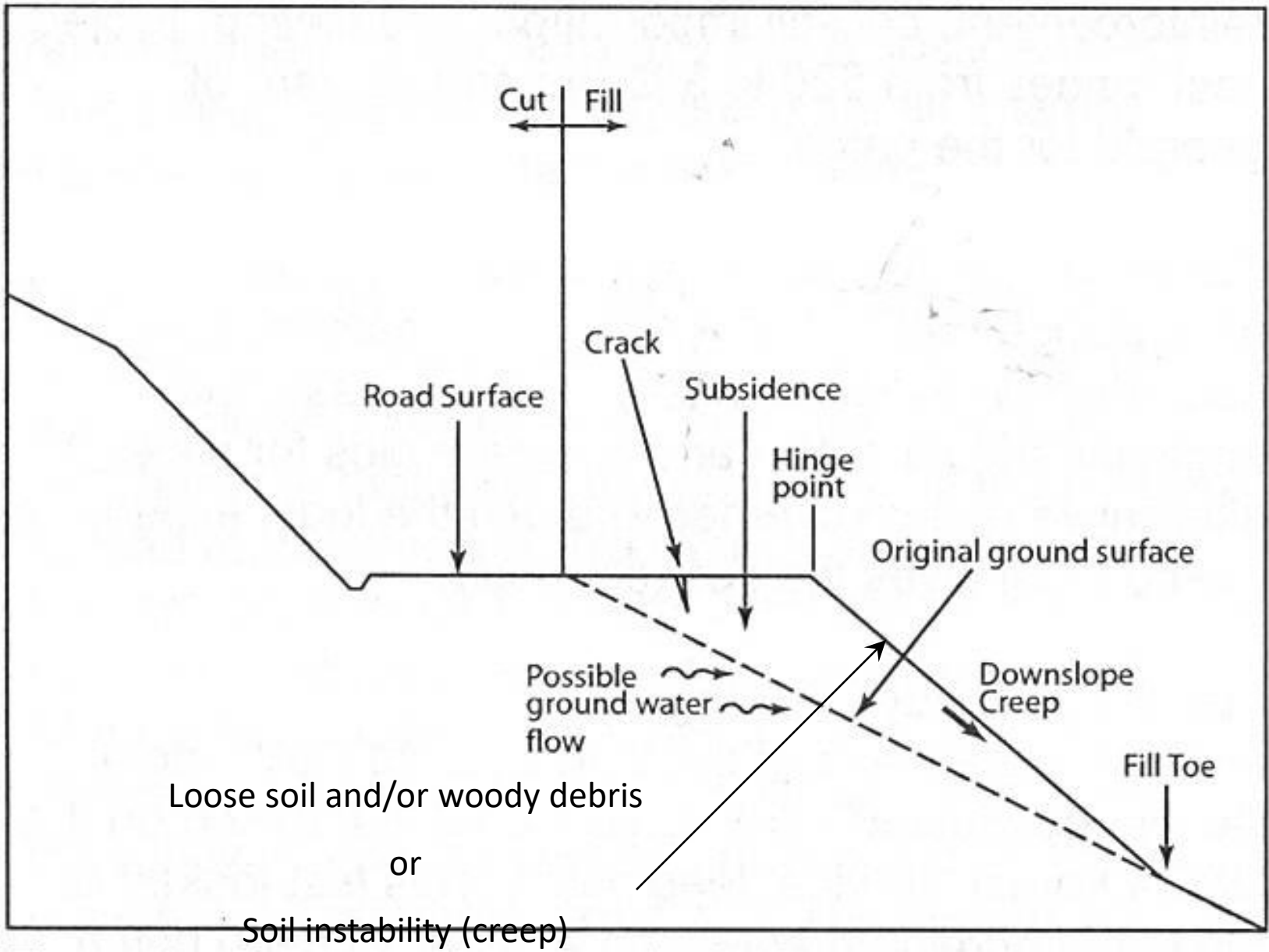
Technology &
Development Program

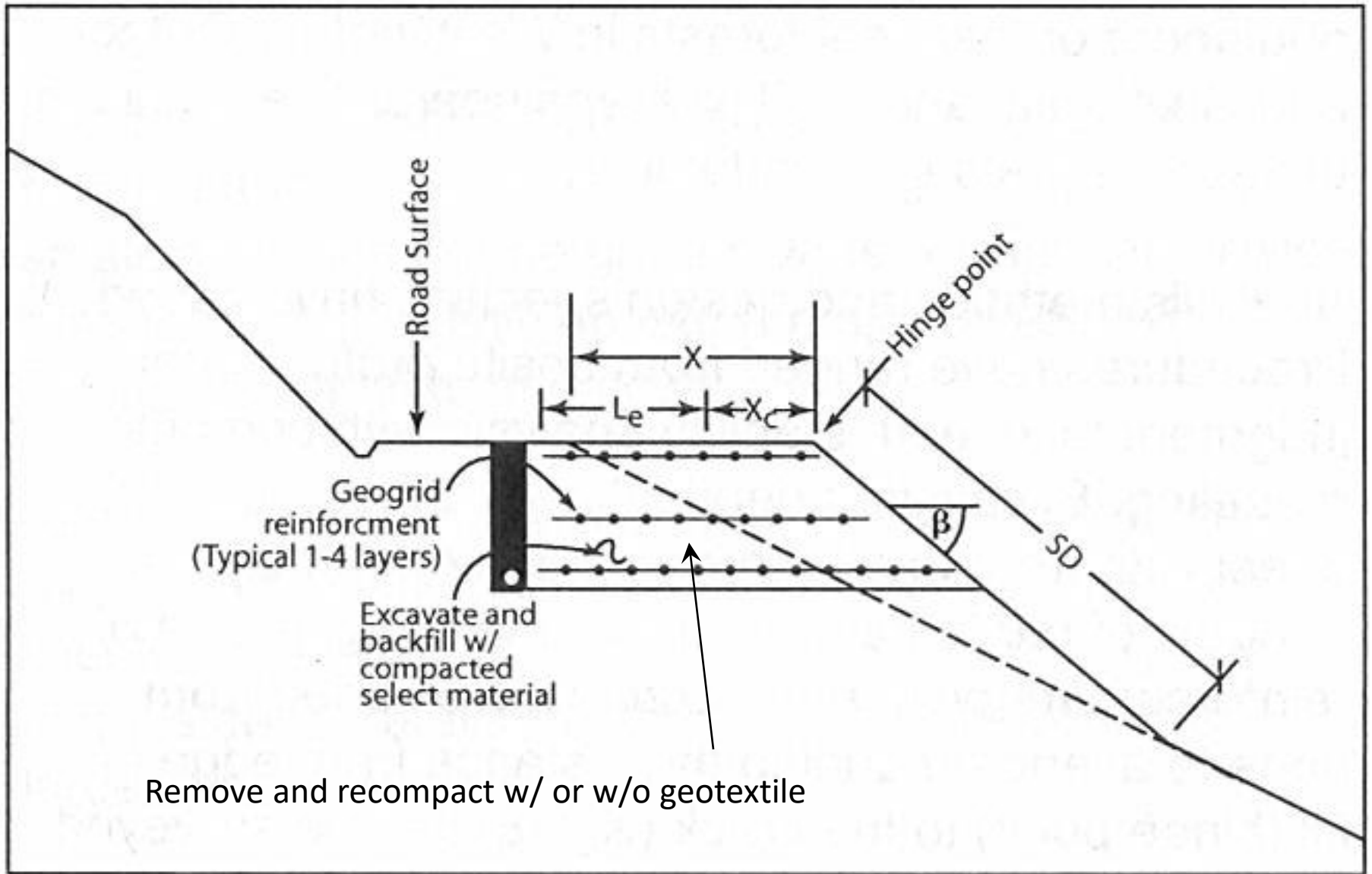
7700—Transportation
Management
October 2005
0577 1204—SDTDC



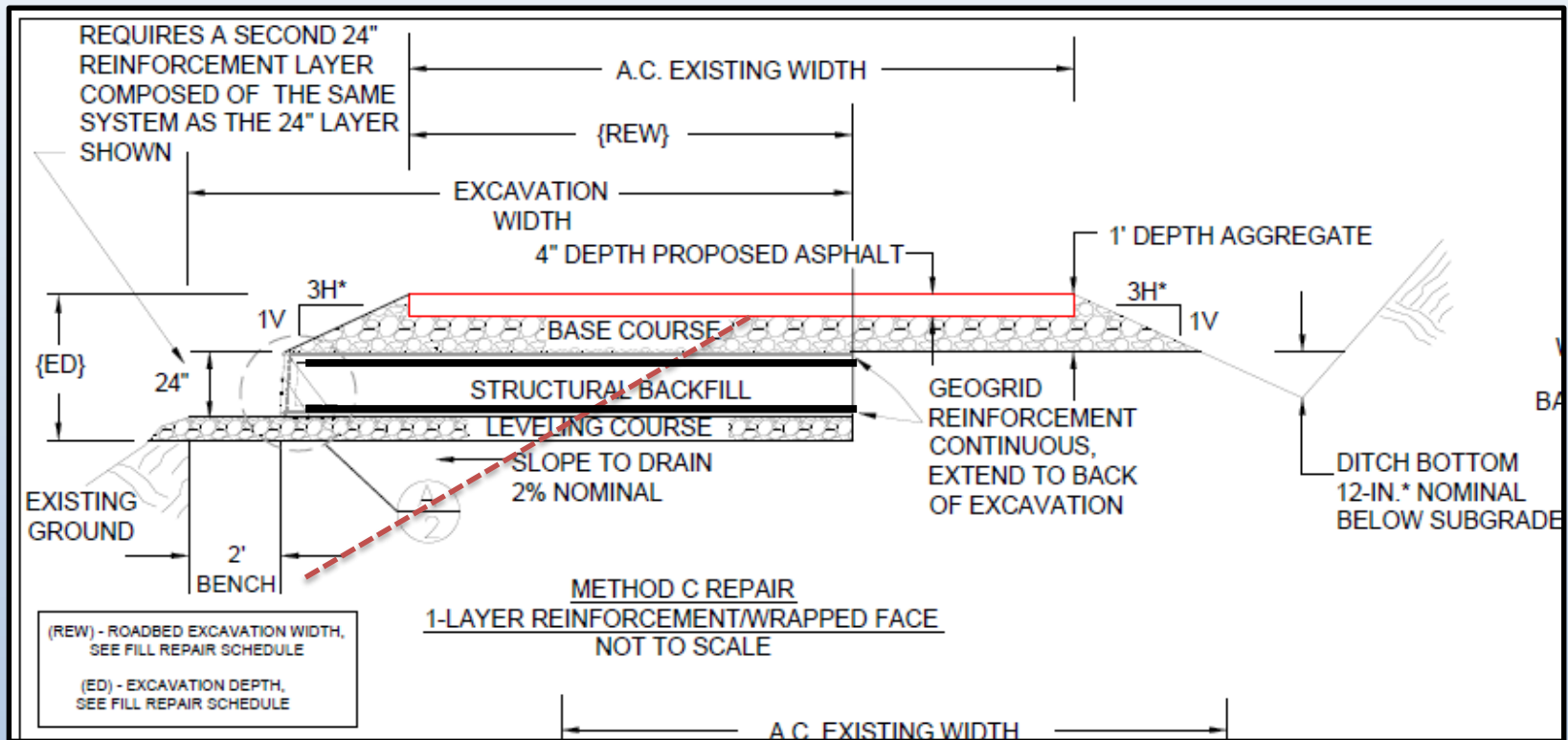
Deep Patch Road Embankment Repair Application Guide







Remove and recompact w/ or w/o geotextile



STABILIZATION W/EARTHWORKS

(REMOVAL - photo from Jigsaw Enterprises)



Typical Buttresses

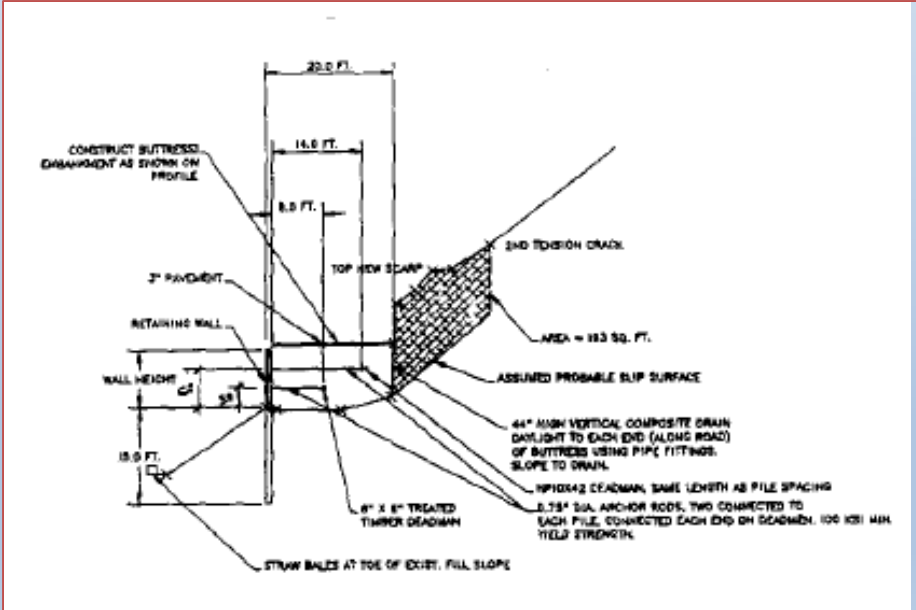
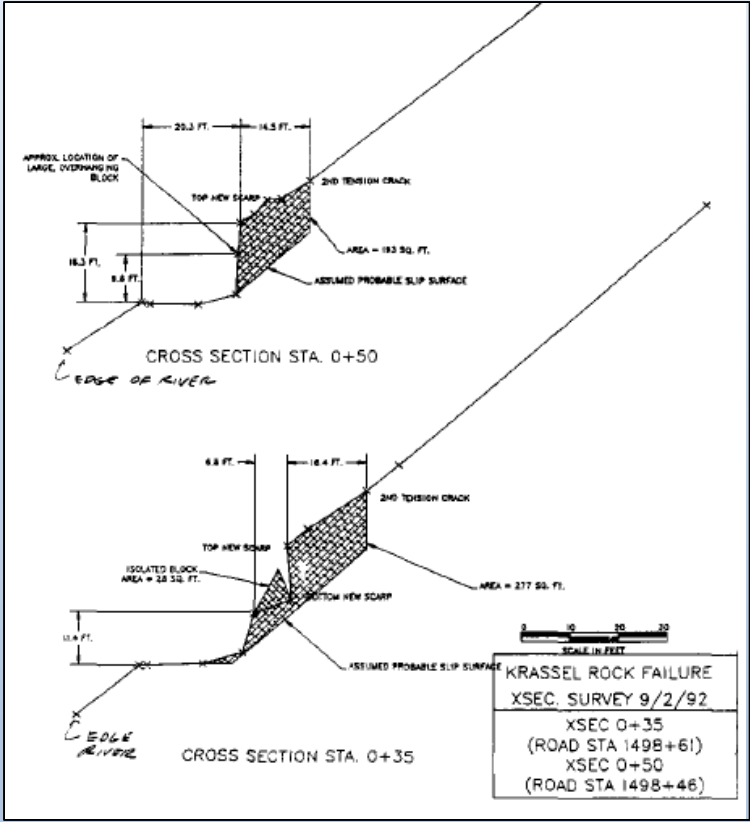
Buttress in Failed Cut-Slope
Shasta Trinity N.F. Region 5



Toe Buttress at Base of Reinforced
Fill Slope, Klamath N. F. Region 5



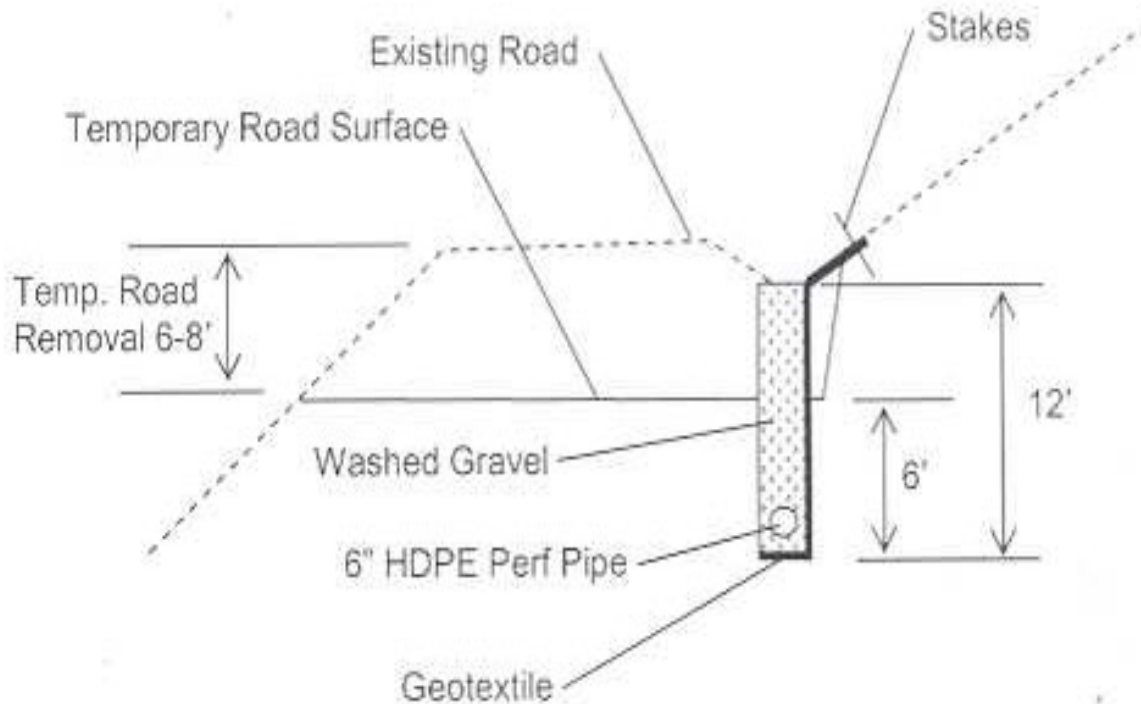
Road as Buttress



STABILIZATION W/DRAINAGE



Cut-Off Drainage Trench Solution



Non-Woven

Water Flow Rate (ASTM D-4491): 80 gpm/sq ft (min)

AOS (ASTM D-4751): 80 (min)

Puncture Strength (ASTM D-48833): 110 lb (min)

Mullen Burst (ASTM D-3786) 350 psi

Coal Creek Landslide Failure

- Seasonal Long Term Creep Failure
- Large amounts of subsurface water
- Previous cross-drain solutions didn't slow movement
- Maintenance crews would add more gravel as a leveling course but over time added load.
- State DNRC wanted to have a timber which required a route on this road.
- Concern about loading on current fill.







10.04.2011

Monitoring Wells

From existing ground surface

Soil Boring/ DCP	Date		
	10-11-2007	5-30-2008	9-2-2010
CC-1	21.1	7.9	16.3
CC-2	27.8	9.8	11.7
CC-3	NG	NG	-
DPS-1	-	0.25	-
DPS-2b	-	0.10	-
DPS-1a	-	NG	-
DPS-2a	-	NG	-

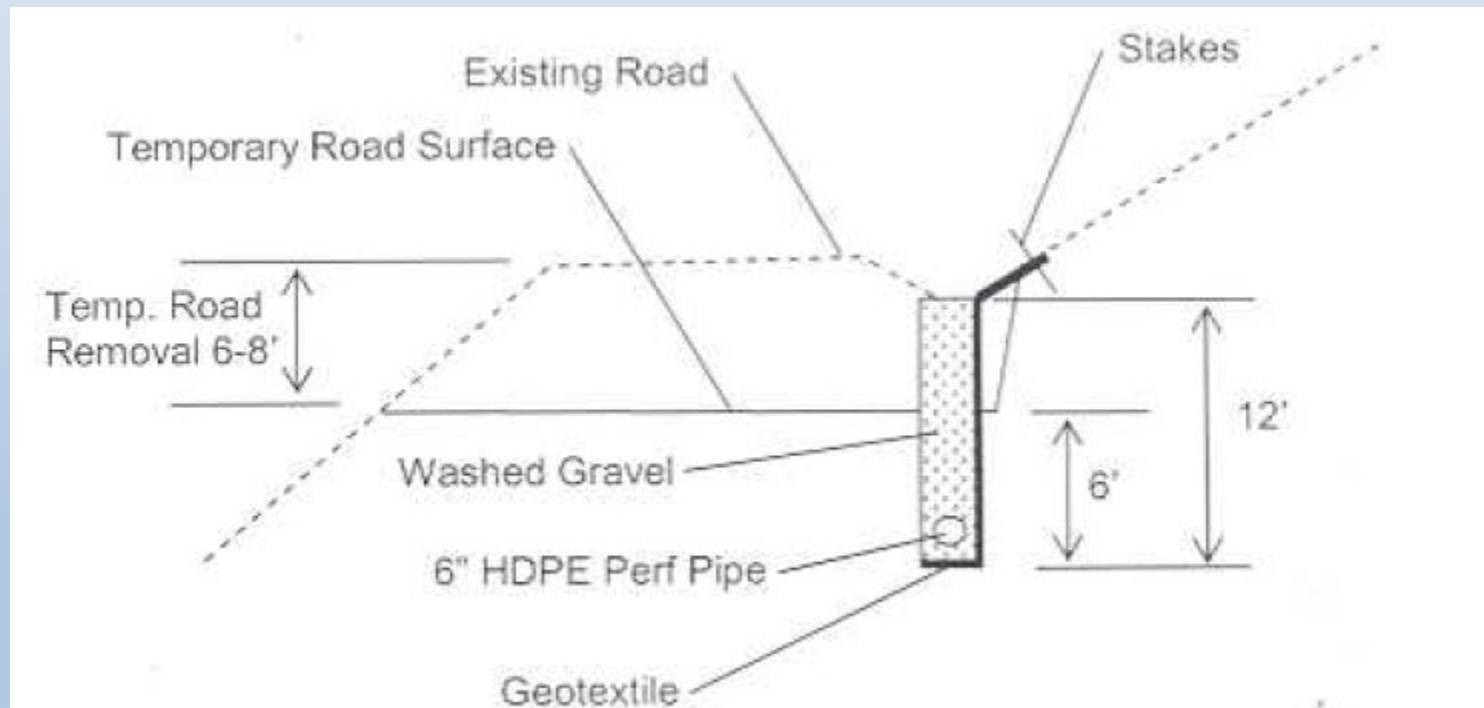
Findings

- High water contents and saturation
- A large presence of fine grained cohesive soils mixed with gravels
- Possible water lenses
- High subsurface water table

Conceptual Design

- Needed to stabilize slope by facilitating drainage given the saturated conditions
- Needed to rebuild the road fill
- Curtain drain was the desired option given no structural stabilizing was needed

Early Conceptual Design

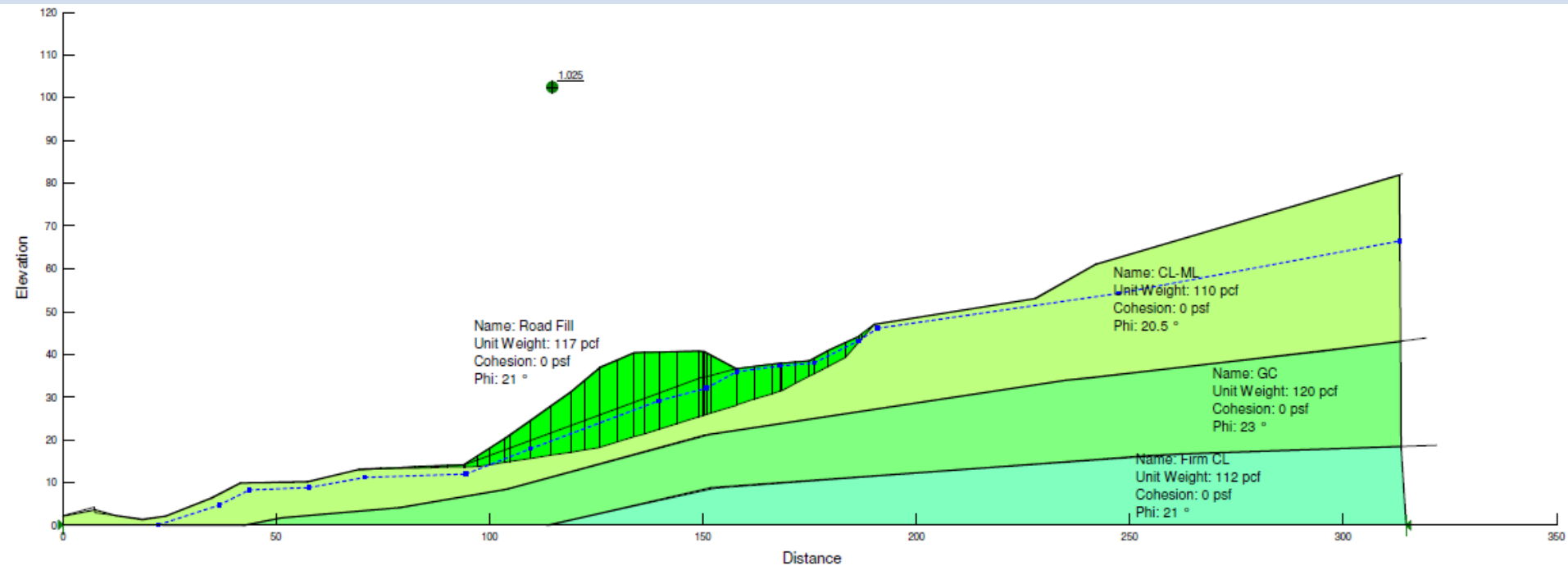


Slope Stability Modeling

- Using field data
 - Come up with a layering system
 - Determine appropriate phreatic surface
 - Failure scarps to tie in a reasonable failure plane
 - Failure plane used to refine soil properties at $FS \sim 1$ for an existing ground model

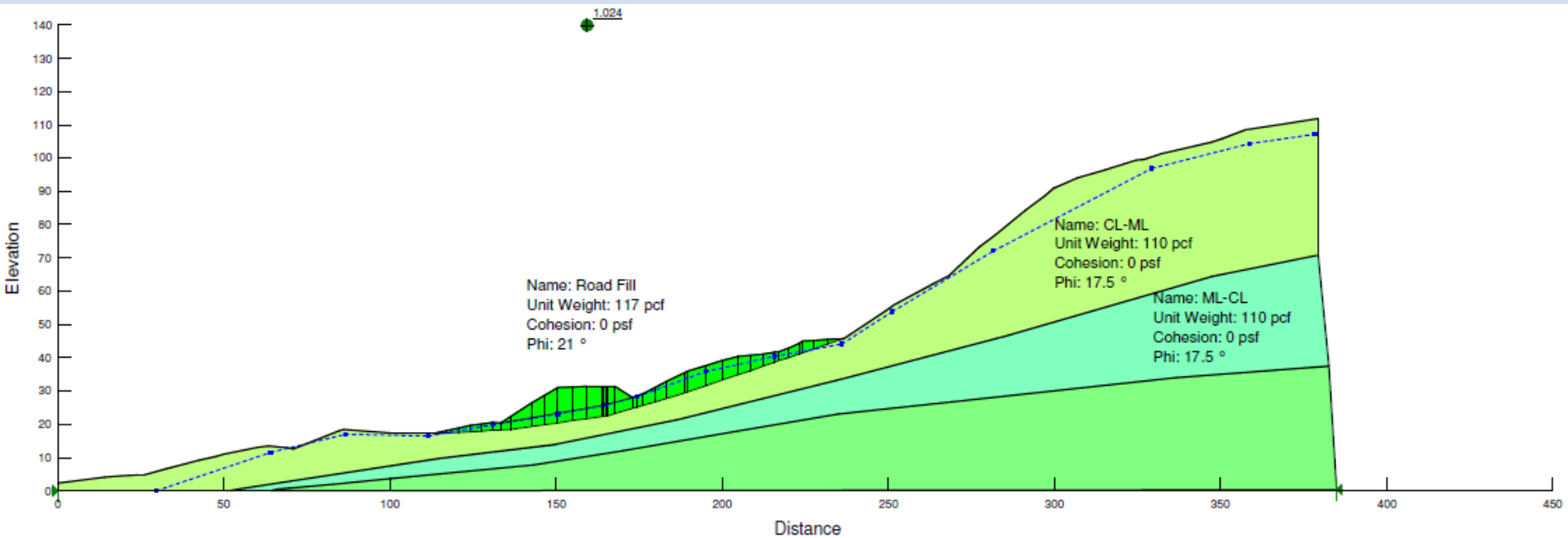
Existing Ground

Station 1+20 – first failure

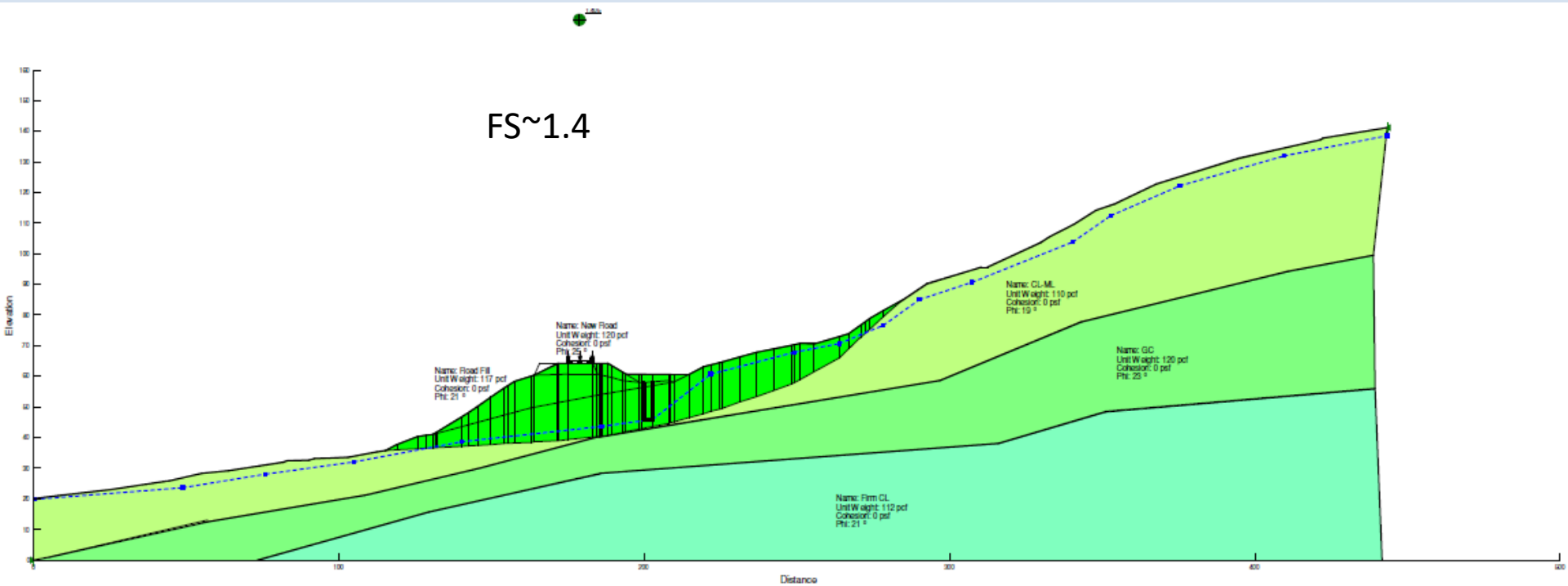


Existing Ground

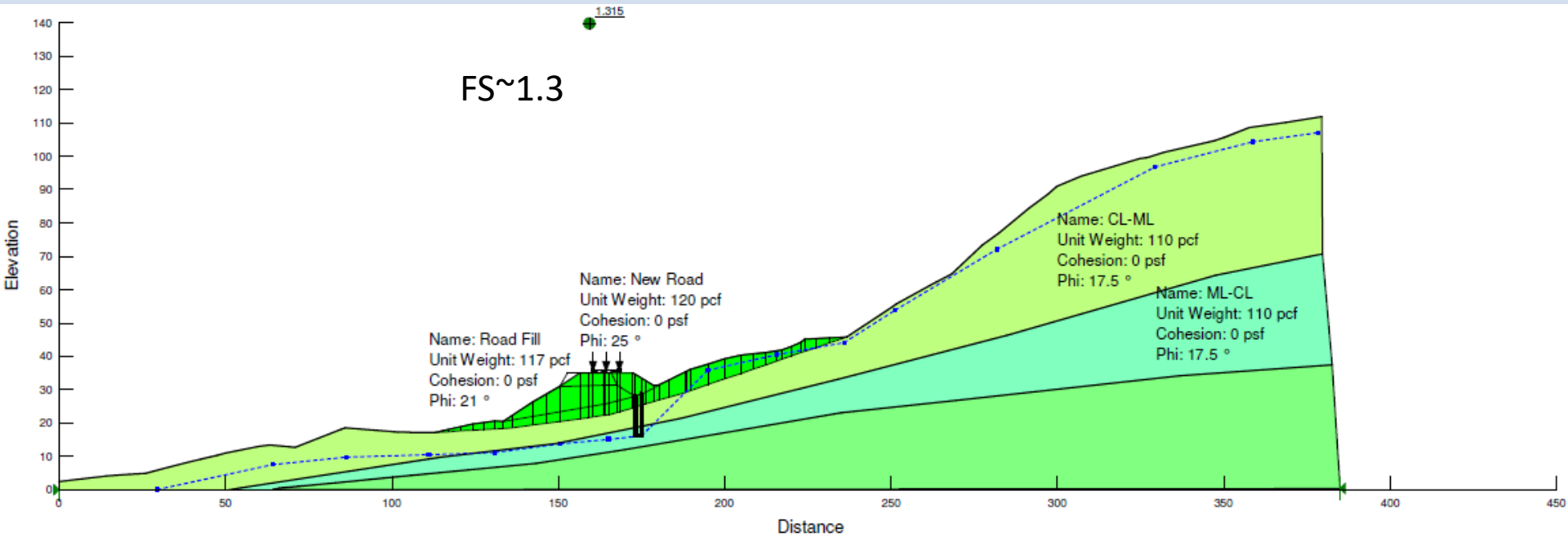
Station 3+00 – second failure



Curtain Drain Analysis



Curtain Drain Analysis



Alternative

Modeled a 14 foot curtain drain to determine increase in factor of safety

- This increased the factor of safety only 0.02
- Opted for the 12 ft depth given the extra cost of excavating an extra two feet



10.05.2011 13:12



10.13.2011



10.13.2011



10.13.2011

Slide Plane!



10.19.2011

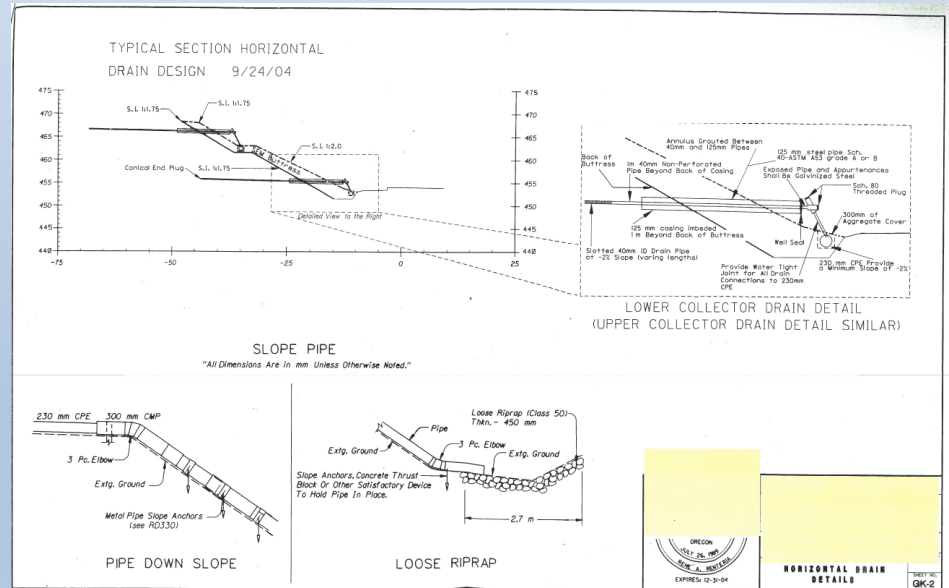
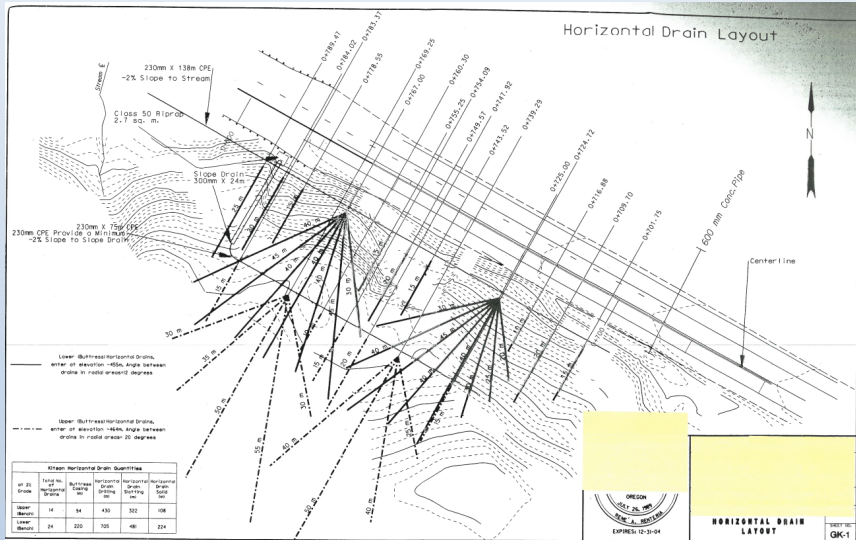


25D

Drill & Install Horizontal Drains



Horizontal Drain Details



COMBINATION METHODS



R1 North Fork Teton Slide

Drainage & Support

(Courtesy Chud Lundgreen, USFS R1)



N Fork Teton - Typical Large Natural Slide



North Fork Teton Slide

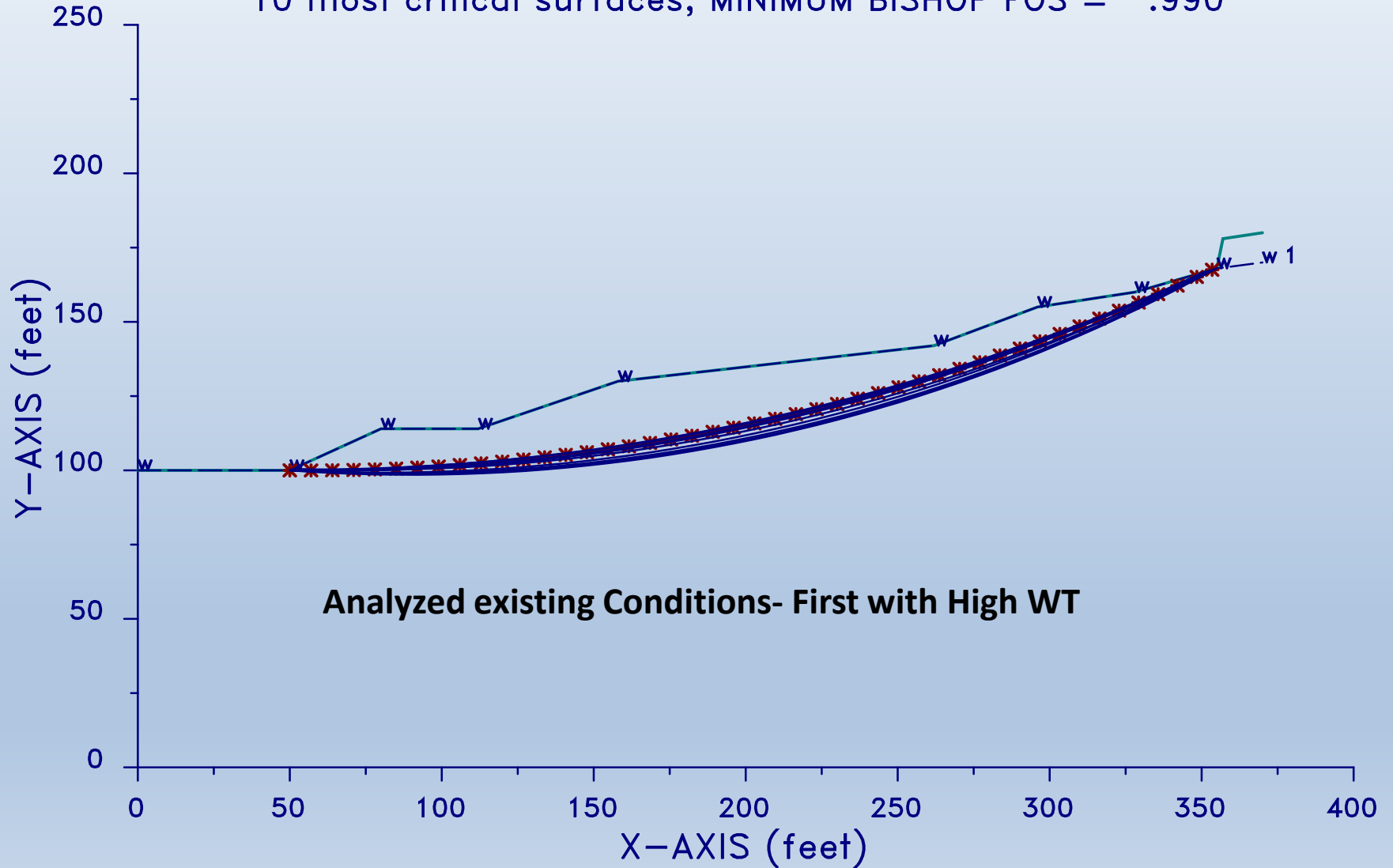
- Ancient slide first disturbed by cutting toe for road during early logging activities.
- Consists of glacial outwash deposit overlaying bedrock in large drainage.
- Disturbed years back and some shallow drainage measures implemented.
- Area burned in 2007 and following Spring run-off, slide re-activated

NF Teton Slide

- Size-300 feet long and 150 feet wide
- Sandy Clay/Gravelly Soil
- Very High Water Table
- Contractor in area and pit-run rock readily available
- Quickest Solution- Rock Buttress and surface drainage.

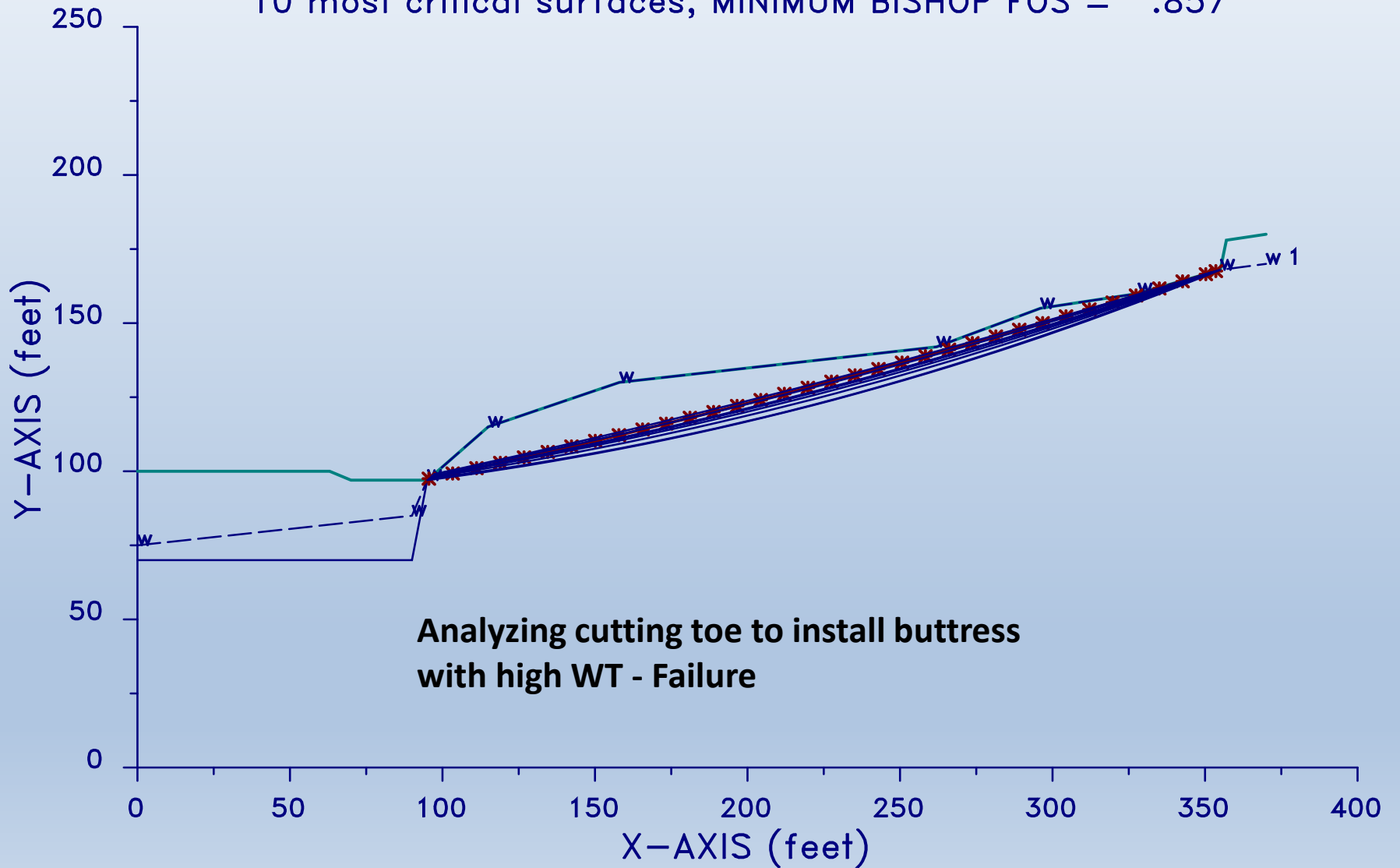
Teton Slump Orig Failure with WT

10 most critical surfaces, MINIMUM BISHOP FOS = .990



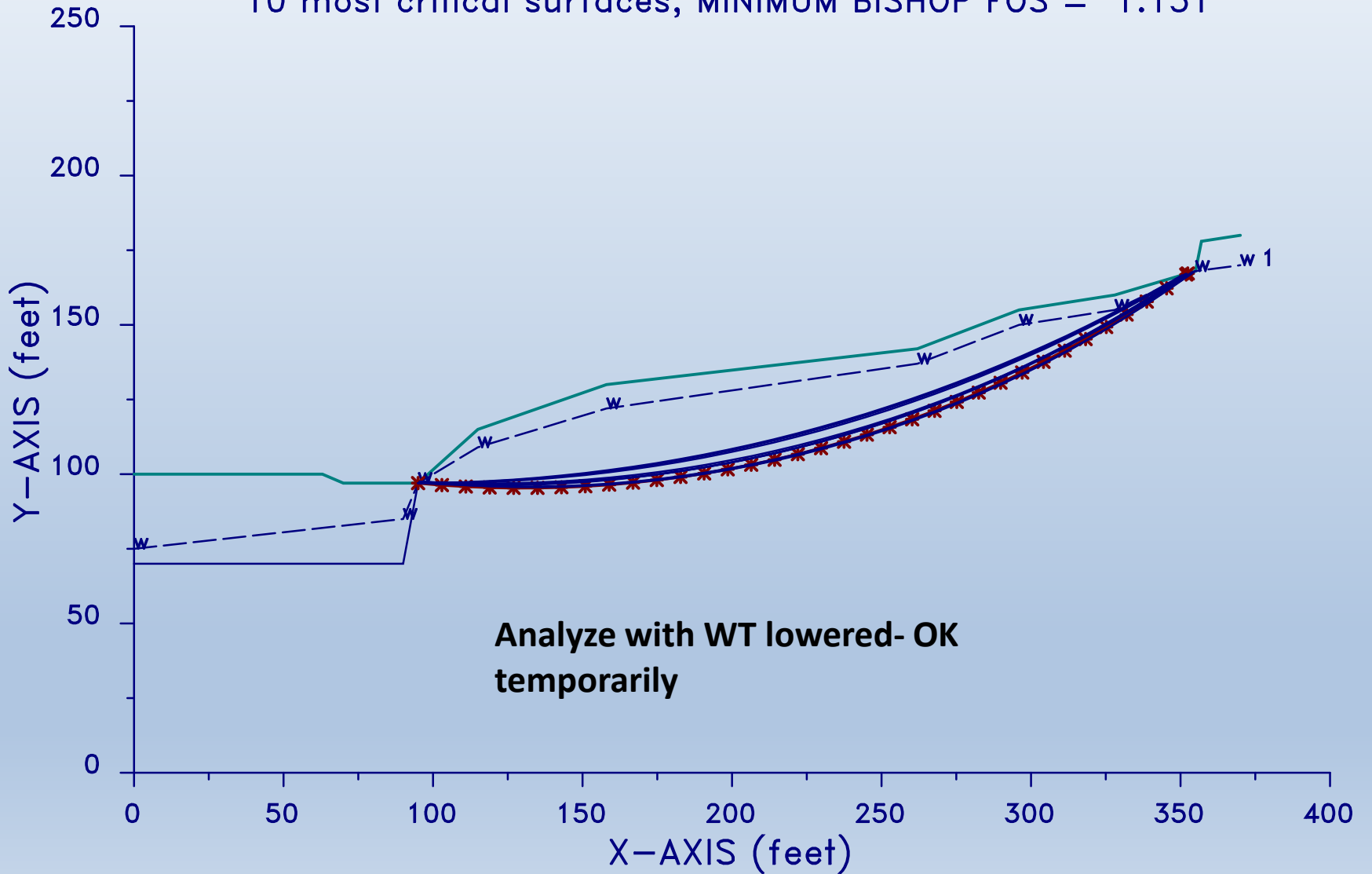
NF Teton Slide Const Cut High WT

10 most critical surfaces, MINIMUM BISHOP FOS = .857



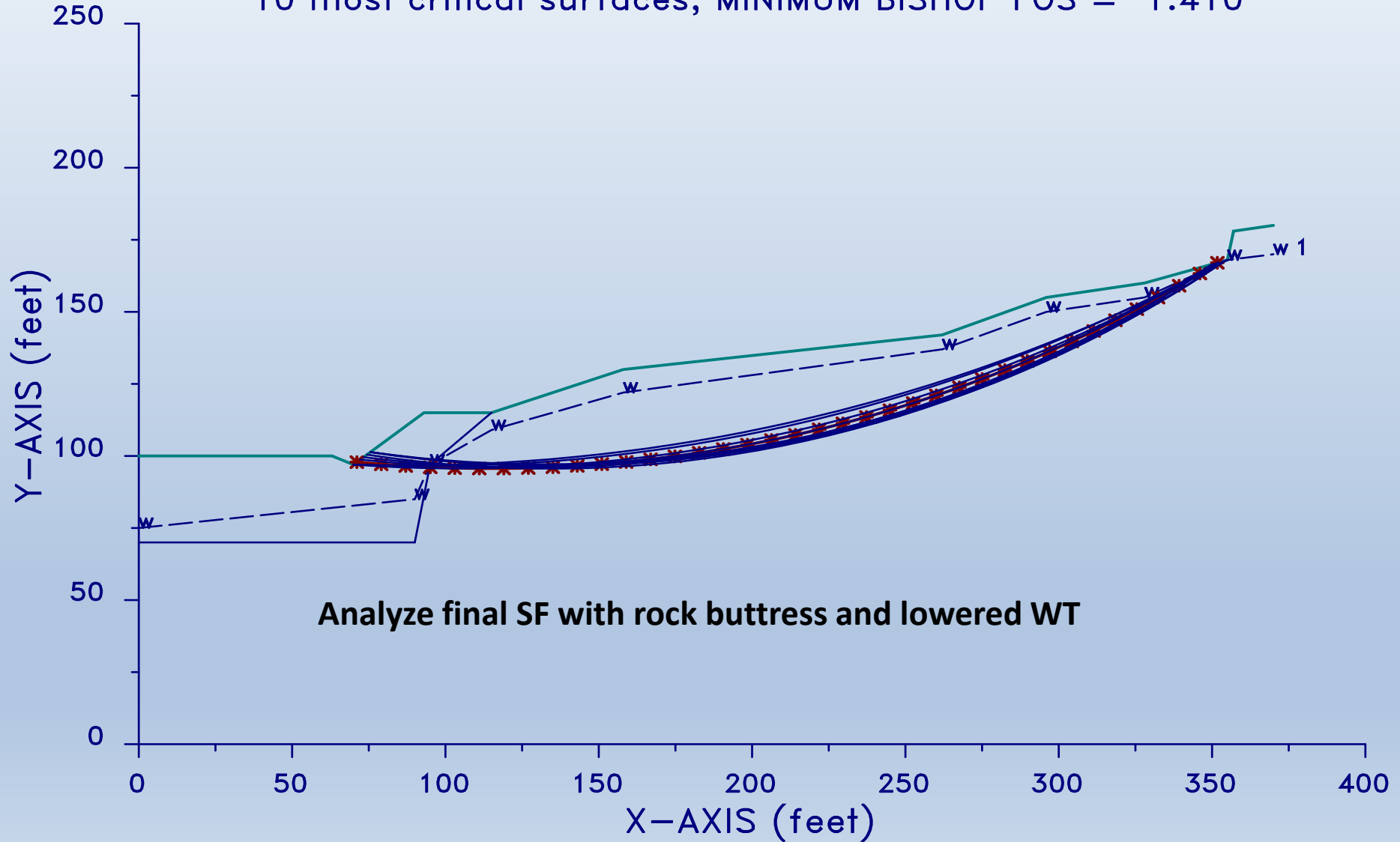
NF Teton Slide Const Cut Low WT

10 most critical surfaces, MINIMUM BISHOP FOS = 1.151

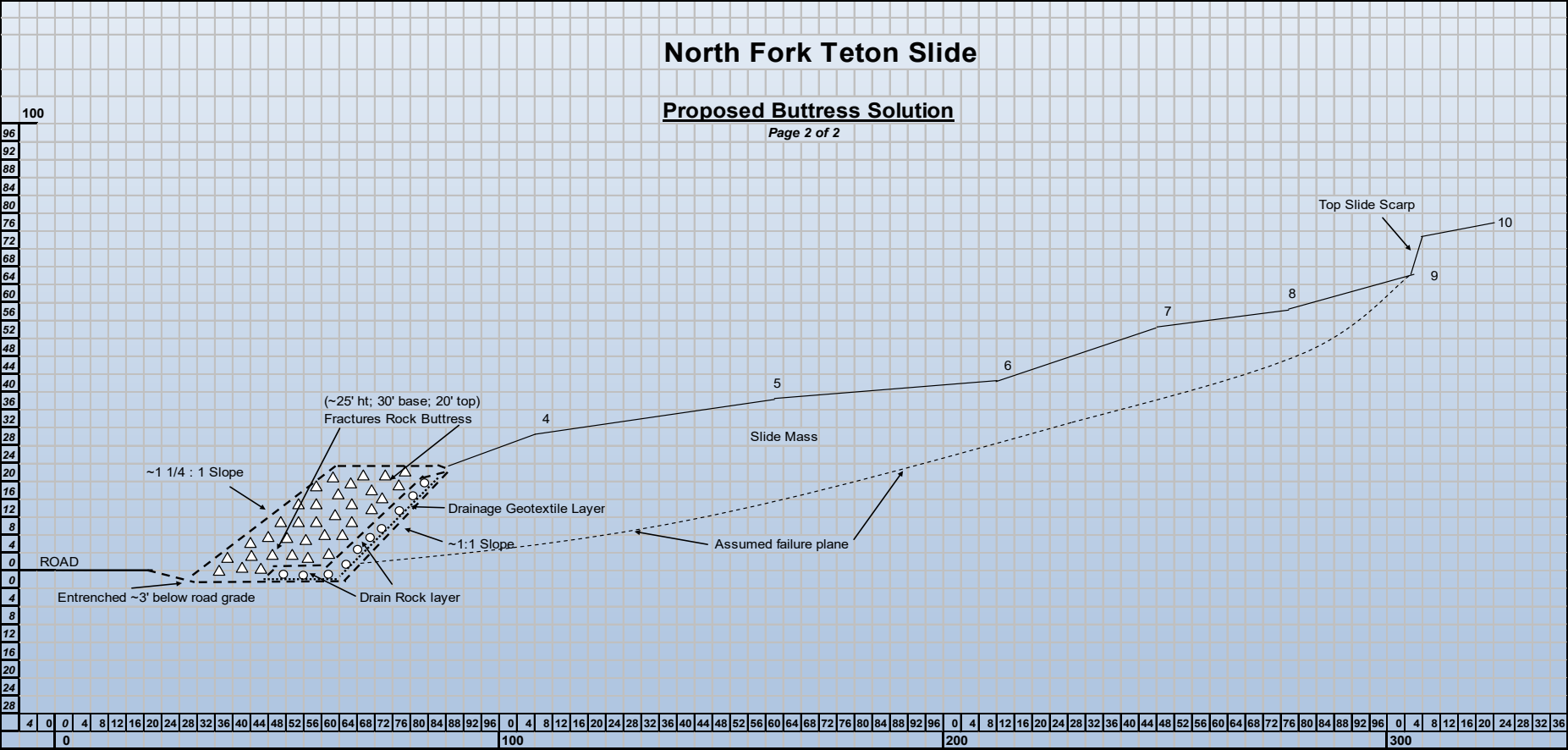


NF Teton Slide Small Buttress-WTlow

10 most critical surfaces, MINIMUM BISHOP FOS = 1.410

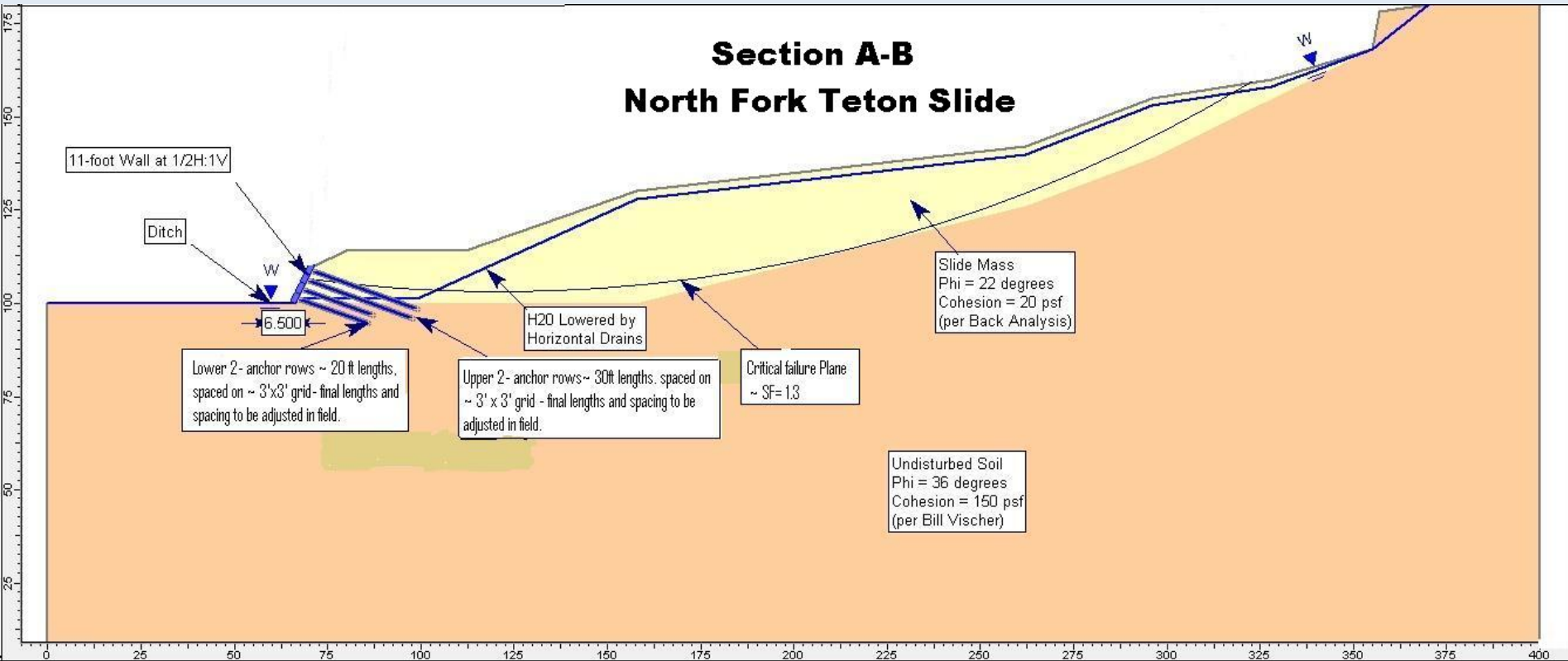


Preliminary Design Proposal Buttress with Surface Trench Drainage



Problem- Surface drainage not lowering WT ???

Final North Fork Teton Design- Soil Nail Buttress Wall at Toe of Slide with Horizontal Drains



Flathead NF Region 1- “Coal Creek” Slides

(Courtesy Chud Lundgreen, USFS R1)



Rebuild the Fill & Drainage

(courtesy Peter Bolander USFS WNF retired)















Field Developed Cross-Section

- **Obtain the following**
 - Slope
 - Relief
 - Landforms
 - Changes in soil and rock units
 - Changes in vegetation
 - Changes in surface water distribution
- **Purpose**
 - 3D model
 - Ability to project known data points

Field Developed Cross Section

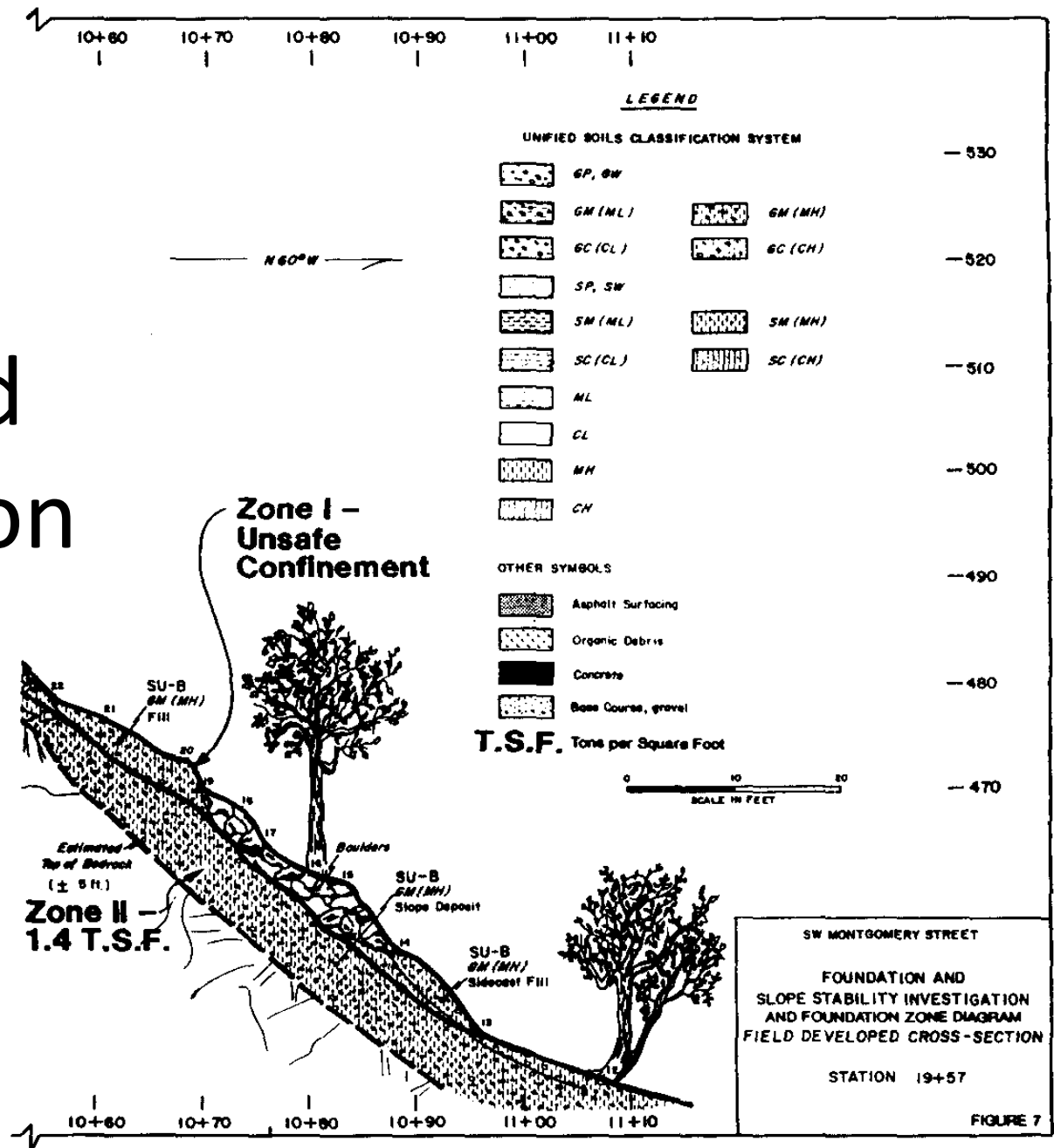


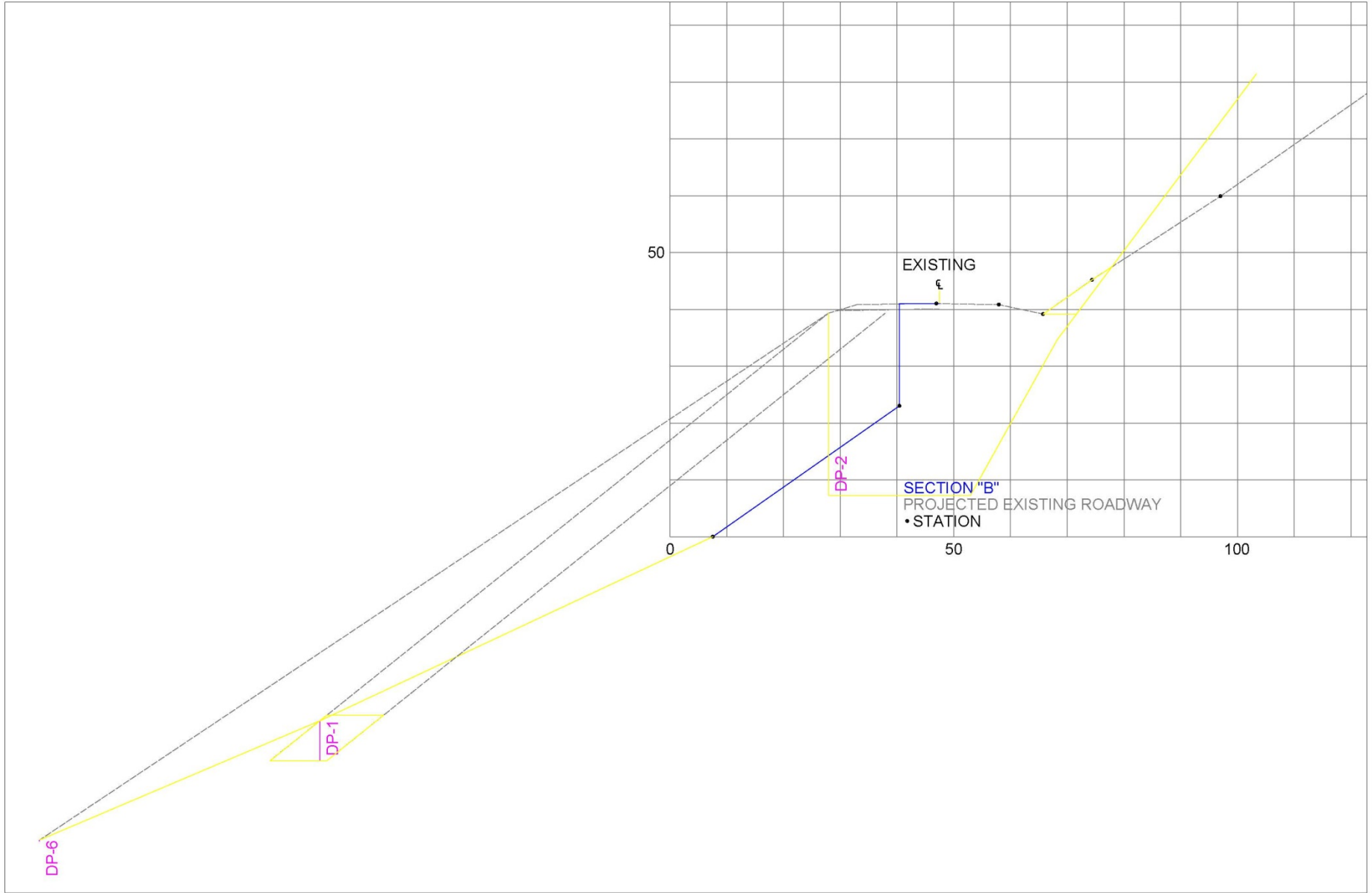
Figure 7. (Continued)

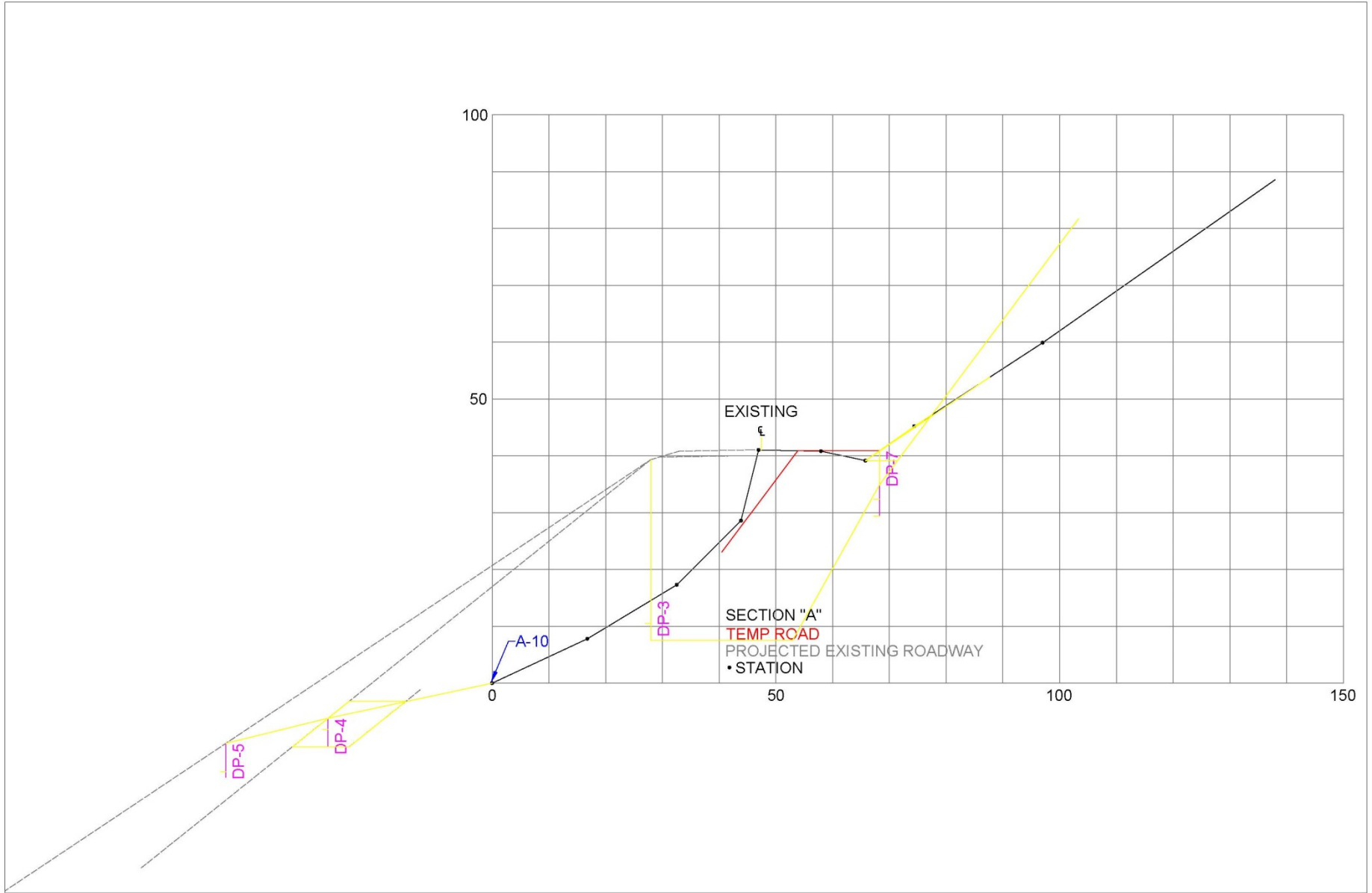
Subsurface Investigation



Final Subsurface Interpretation

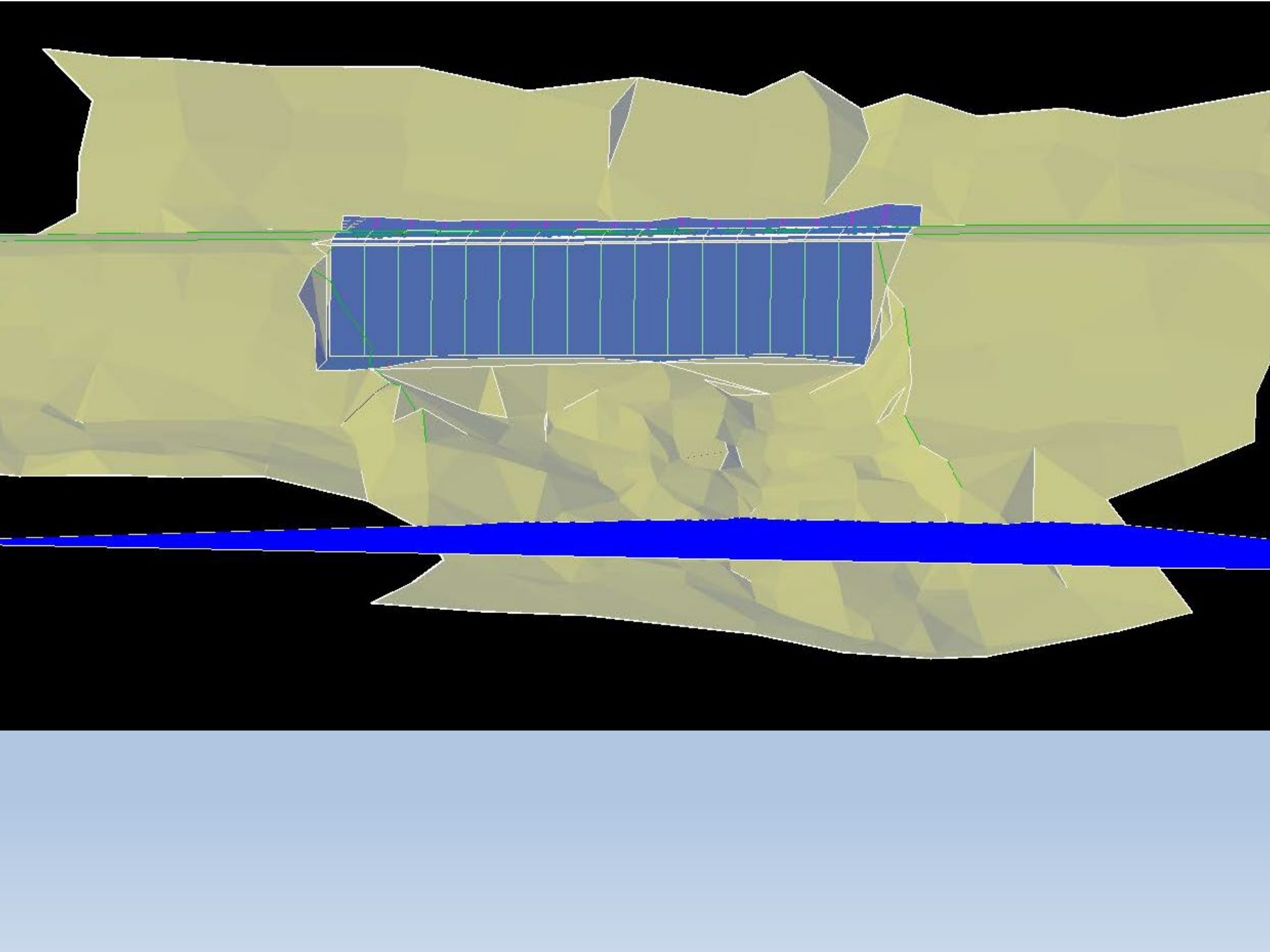
- **Based on surface and drive probe information only**
- **See following “Geologic Cross-Sections”**

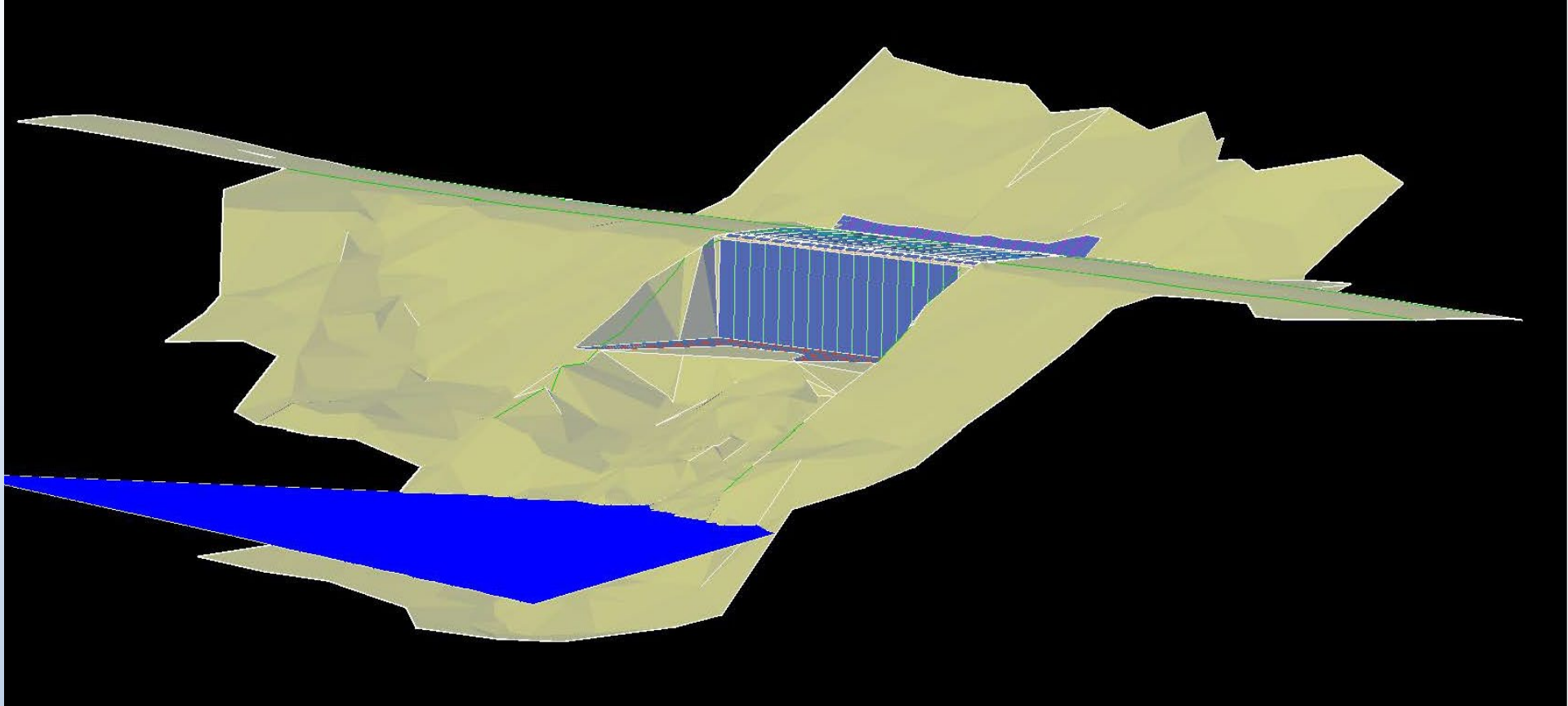


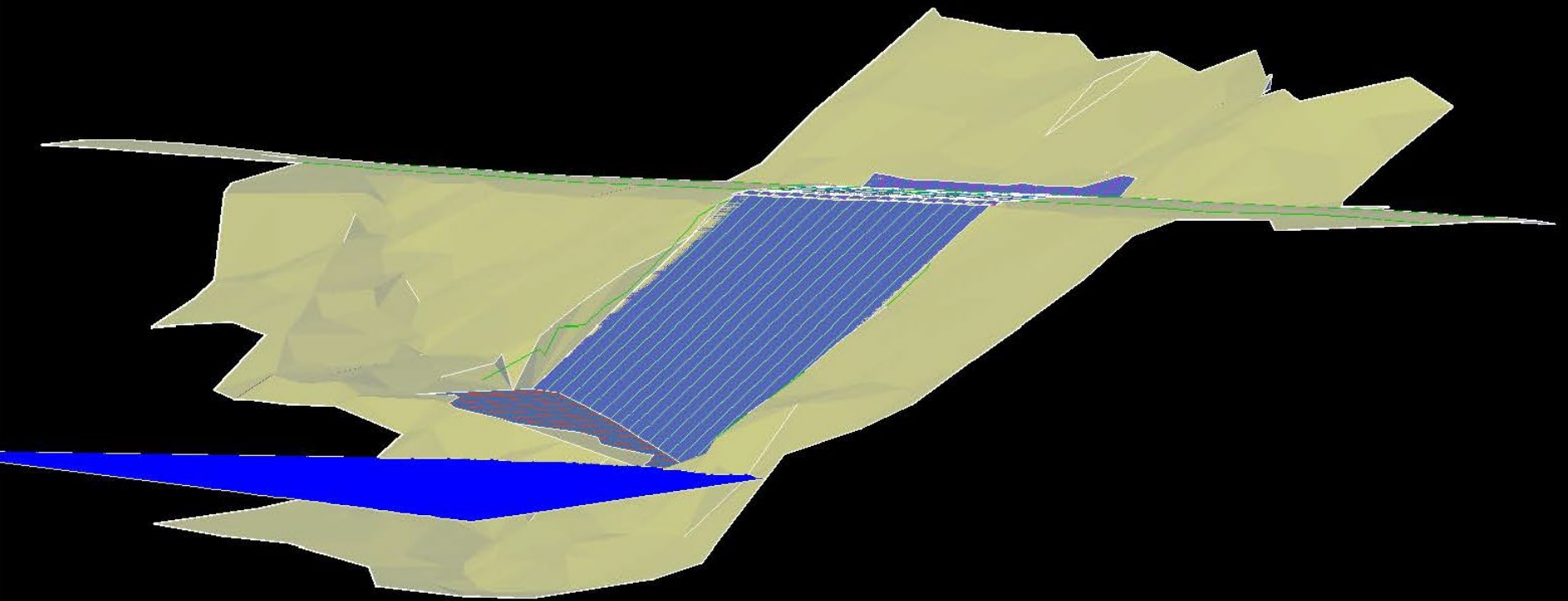


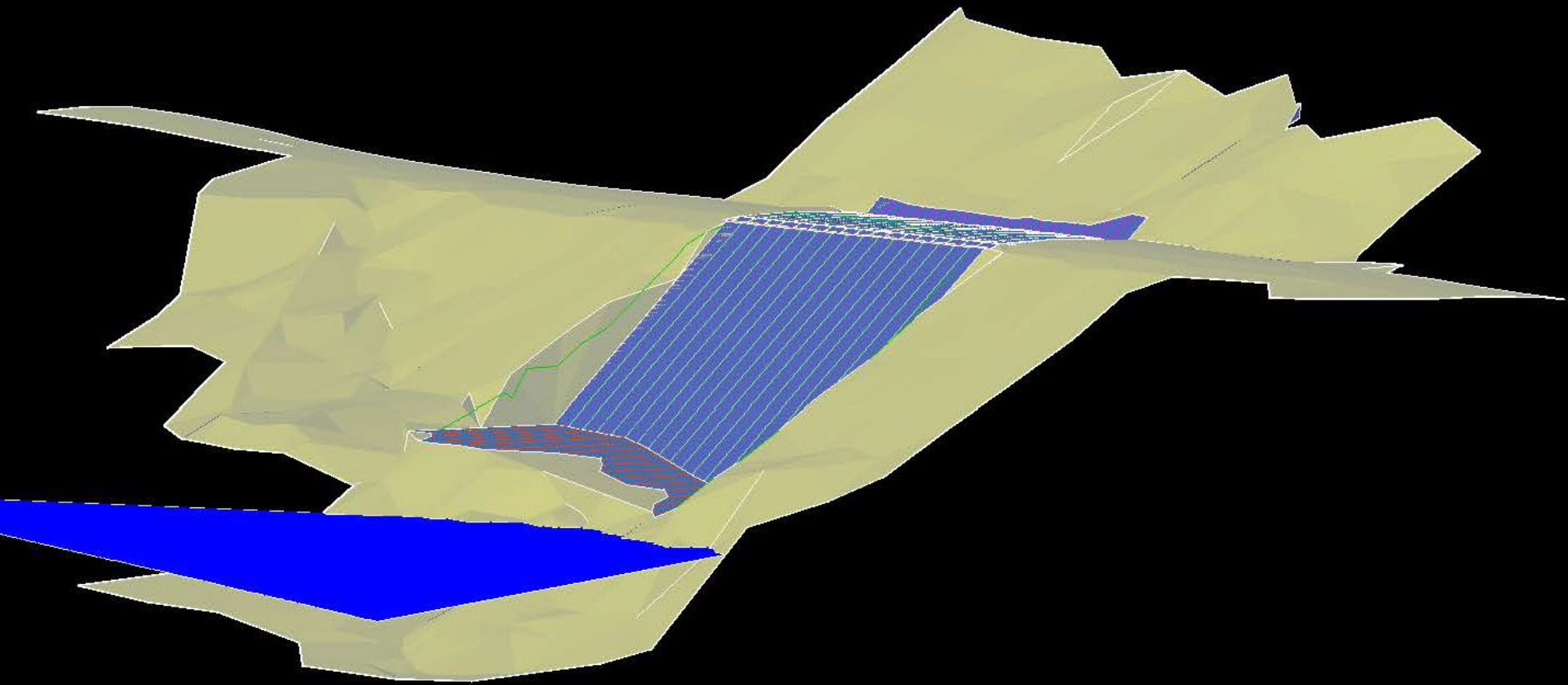
Repair Alternatives

- **Road Closure/Alternate Route**
- **Realignment**
- **Earth Embankment**
- **Rip Rap Embankment**
- **Reinforced Soil Slope**
- **Retaining Wall**







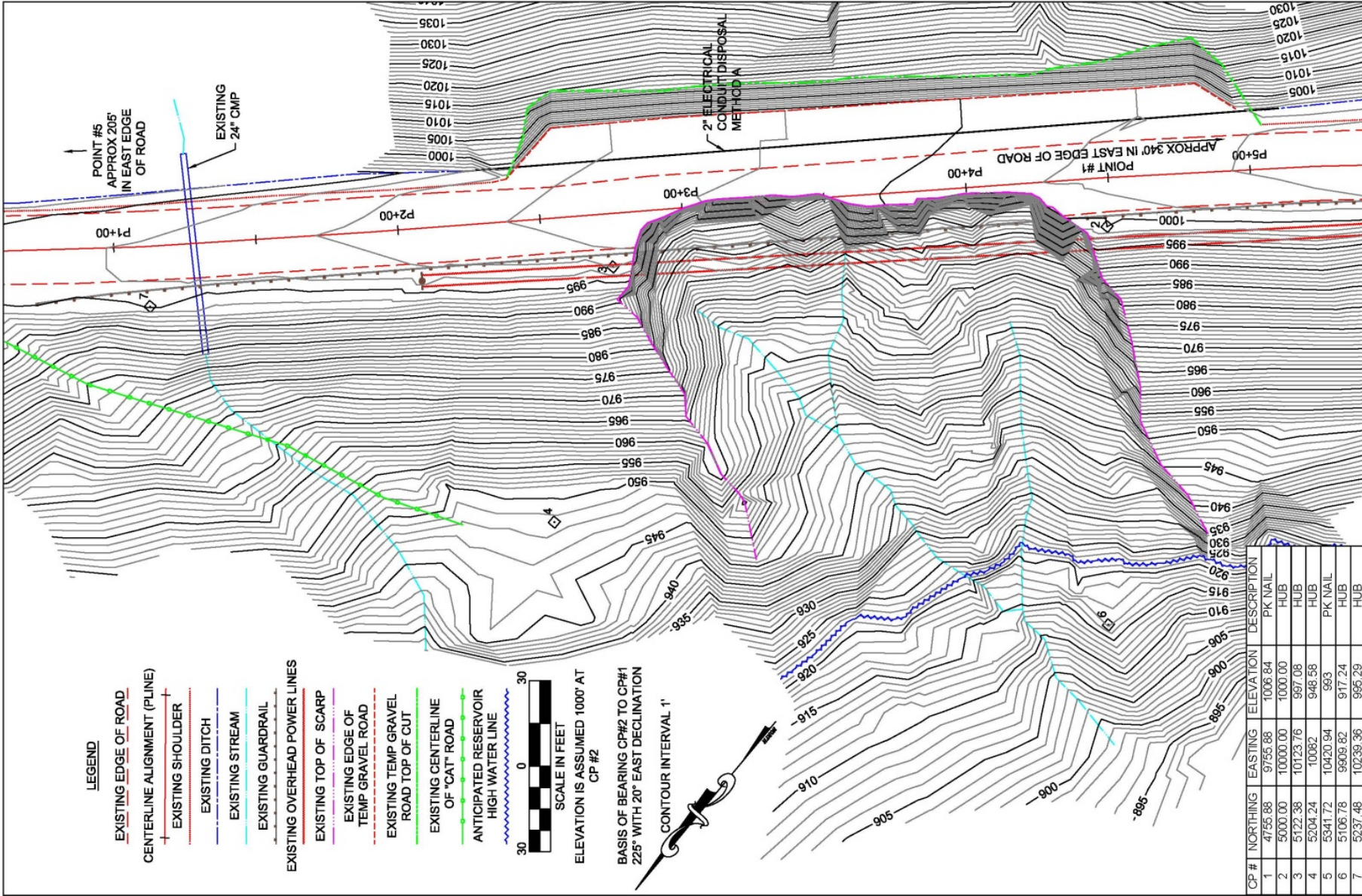


Repair Alternatives

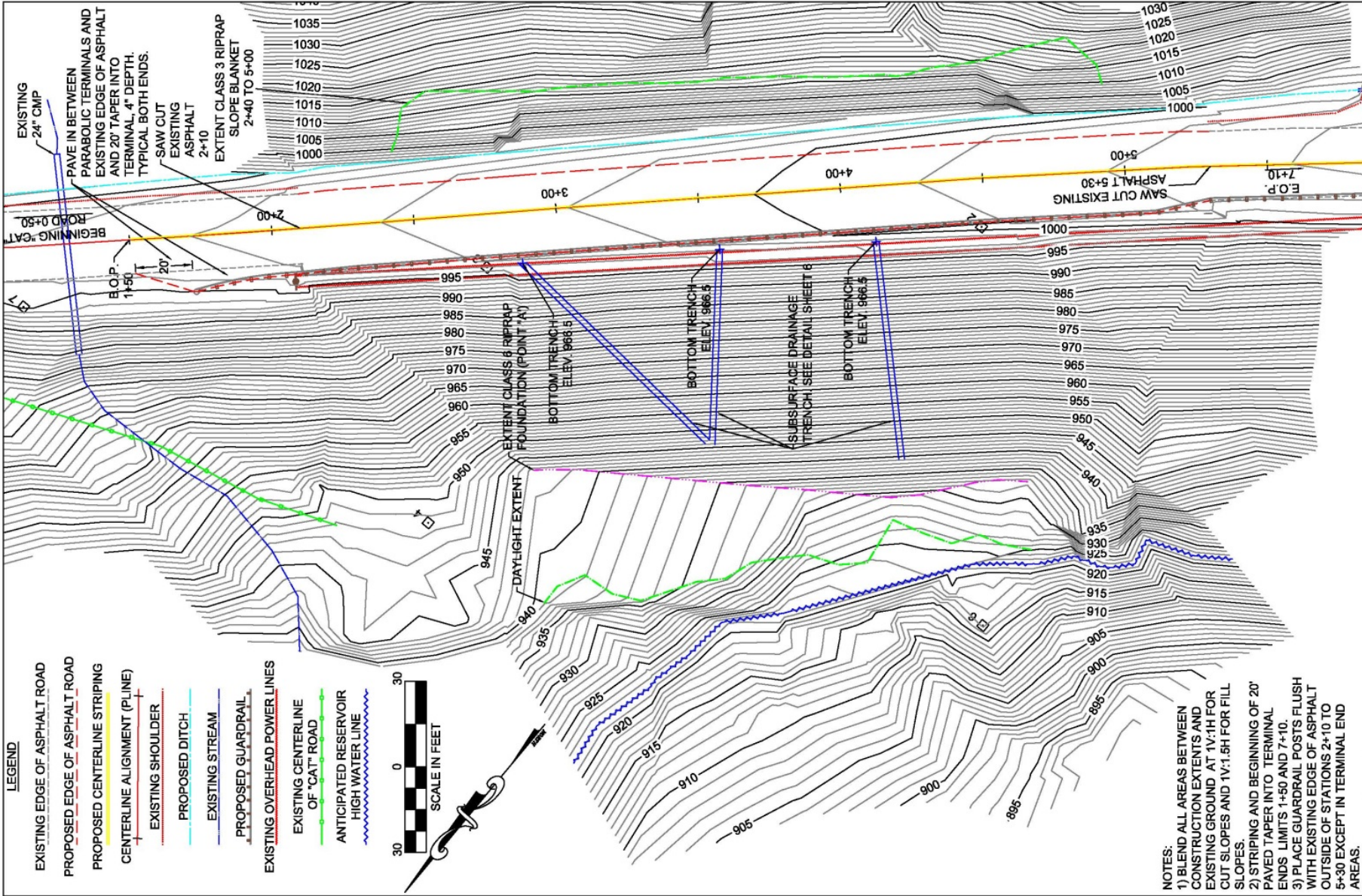
Alternative	Pro	Con	Relative Costs
1.25H to 1V Rip Rap Embankment	* Stay out of Reservoir		Low
1H to 1V Rip Rap Embankment		* Toe within Reservoir	Low
Retaining Wall	* Stay out of reservoir	* Could not provide temporary access during construction	High
Reinforced Soil Slope	* Stay out of reservoir	* Could not use excavated material	Medium
Full Alignment Shift Into the Hillside		* Unsure if would encounter additional subsurface water	Low
Partial Alignment Shift into the Hillside and either one of the above Fillslope Repairs Options	* Stay out of reservoir	* Difficult to provide temporary access during construction	Medium

Design

- **Stable Foundation**
- **Drainage**
- **Stable Embankment**
- **Access During Construction**
- **Recreation Traffic Considerations**



CP #	NORTHING	EASTING	ELEVATION	DESCRIPTION
1	4755.88	9755.88	1006.84	PK NAIL
2	5000.00	10000.00	1000.00	HUB
3	5122.38	10123.76	997.08	HUB
4	5204.24	10082	948.58	HUB
5	5341.72	10420.94	993	PK NAIL
6	5106.78	9909.82	917.24	HUB
7	5237.48	10239.36	956.29	HUB



Construction

- **Confirm Foundation Assumptions**
- **Drainage Considerations**

















Lessons Learned

- **Creating 3-D subsurface models improve the selection of alternatives with higher degree of confidence and fewer design modifications**
- **Team effort between geotech and designer leads to quick contract package and award**
- **For critical designed slopes check the contractor for accuracy**
- **Can use same process for evaluation of retaining walls and initial rock source evaluation**

More Info and Examples...

United States
Department of
Agriculture

Forest Service

Engineering Staff

Washington, DC

EM-7170-13

August 1994

Slope Stability Reference Guide for National Forests in the United States

Volume III

